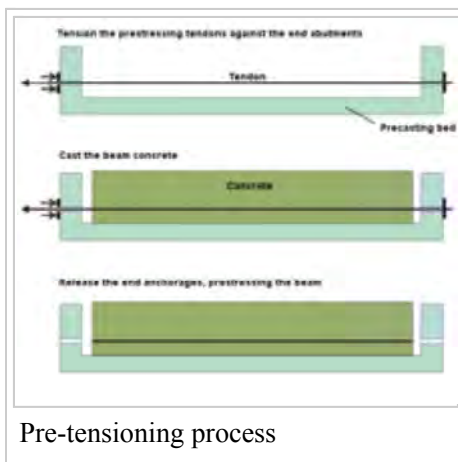
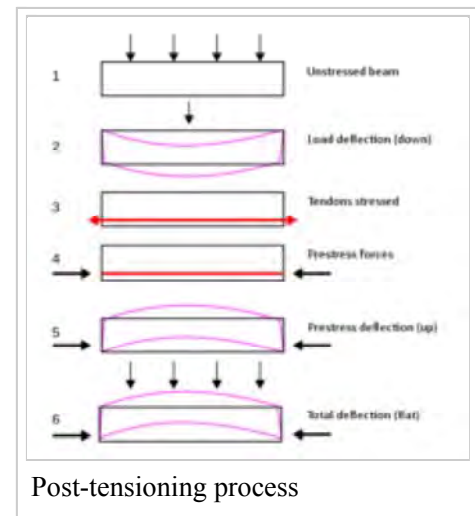


# Prestressed concrete

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**Prestressed concrete** is a concrete construction material which is placed under compression prior to it supporting any applied loads (i.e. it is "pre" stressed).<sup>[1][2]:3–5</sup> A more technical definition is "*Structural concrete in which internal stresses have been introduced to reduce potential tensile stresses in the concrete resulting from loads.*"<sup>[3]</sup> This compression is produced by the tensioning of high-strength "tendons" located within or adjacent to the concrete volume, and is done to improve the performance of the concrete in service.<sup>[4]</sup> Tendons may consist of single wires, multi-wire strands or threaded bars, and are most commonly made from high-tensile steels, carbon fibre or aramid fibre.

<sup>[1]:52–59</sup> The essence of prestressed concrete is that once the initial compression has been applied, the resulting material has the characteristics of high-strength concrete when subject to any subsequent compression forces, and of ductile high-strength steel when subject to tension forces. This can result in improved structural capacity and/or serviceability compared to conventionally reinforced concrete in many situations.<sup>[2]:6[5]</sup>



Prestressed concrete is used in a wide range of building and civil structures where its improved concrete performance can allow longer spans, reduced structural thicknesses, and material savings to be realised compared to reinforced concrete. Typical applications range through high-rise buildings, residential slabs, foundation systems, bridge and dam structures, silos and tanks, industrial pavements and nuclear containment structures.<sup>[6]</sup>

First used in the late-nineteenth century,<sup>[1]</sup> prestressed concrete has developed to encompass a wide range of technologies. Tensioning (or "stressing") of the tendons may be undertaken either *before* (pre-tensioning) or *after* (post-tensioning) the concrete itself is cast. Tendons may be located either *within* the

concrete volume (internal prestressing), or wholly *outside* of it (external prestressing). Whereas pre-tensioned concrete by definition uses tendons directly bonded to the concrete, post-tensioned concrete can use either *bonded* or *unbonded* tendons. Finally, tensioning systems can be classed as either *monostrand* systems, where each tendon's strand or wire is stressed individually, or *multi-strand* systems where all strands or wires in a tendon are stressed simultaneously.<sup>[5]</sup>

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## Pre-tensioned concrete

Pre-tensioned concrete is a variant of prestressed concrete where the tendons are tensioned *prior* to the concrete being cast.<sup>[1]:25</sup> The concrete bonds to the tendons as it cures, following which the end-anchoring of the tendons is released, and the tendon tension forces are transferred to the concrete as compression by static friction.<sup>[5]:7</sup>

Pre-tensioning is a common prefabrication technique, where the resulting concrete element is manufactured remotely from the final structure location and transported to site once cured. It requires strong, stable end-anchorage points between which the tendons are stretched. These anchorages form the ends of a "casting bed" which may be many times the length of the concrete element being fabricated. This allows multiple elements to be constructed end-on-end in the one pre-tensioning operation, allowing significant productivity benefits and economies of scale to be realised for this method of construction.<sup>[5][7]</sup>

The amount of bond (or adhesion) achievable between the freshly set concrete and the surface of the tendons is critical to the pre-tensioning process, as it determines when the tendon anchorages can be safely released. Higher bond strength in early-



Pre-tensioned bridge girder in precasting bed. Note single-strand tendons exiting through formwork

age concrete allows more economical fabrication as it speeds production. To promote this, pre-tensioned tendons are usually composed of isolated *single* wires or strands, as this provides a greater surface area for bond action than bundled strand tendons.<sup>[5]</sup>



Pre-tensioned hollow-core plank being placed

Unlike those of post-tensioned concrete, the tendons of pre-tensioned concrete elements generally form straight lines between end-anchorage. Where "profiled" or "harped" tendons<sup>[8]</sup> are required, one or more intermediate *deviators* are located between the ends of the tendon to hold the tendon to the desired non-linear alignment during tensioning.<sup>[1]:68–73[5]:11</sup> Such deviators usually act against substantial forces, and hence require a robust casting bed foundation system. Straight tendons are typically used in "linear" precast elements such as shallow beams, hollow-core planks and slabs, whereas profiled tendons are more commonly found in deeper precast bridge beams and girders.

Pre-tensioned concrete is most commonly used for the fabrication of structural beams, floor slabs, hollow-core planks, balconies, lintels, driven piles, water tanks and concrete pipes.

## Post-tensioned concrete

Post-tensioned concrete is a variant of prestressed concrete where the tendons are tensioned *after* the surrounding concrete structure has been cast.<sup>[1]:25</sup>

The tendons are not placed in direct contact with the concrete, but are encapsulated within a protective sleeve or duct which is either cast into the concrete structure or placed adjacent to it. At each end of a tendon is an anchorage assembly firmly fixed to the surrounding concrete. Once the concrete has been cast and set, the tendons are tensioned ("stressed") by pulling the tendon ends through the anchorages while pressing against the concrete. The large forces required to tension the tendons result in a significant permanent compression being applied to the concrete once the tendon is "locked-off" at the anchorage.<sup>[1]:25[5]:7</sup> The method of locking the tendon-ends to the anchorage is dependent upon the tendon composition, with the most common systems being "button-head" anchoring (for wire tendons), split-wedge anchoring (for strand tendons), and threaded anchoring (for bar tendons).<sup>[1]:79–84</sup>



Post-tensioned tendon anchorage. Four-piece "lock-off" wedges are visible holding each strand



Balanced-cantilever bridge under construction. Each added segment is supported by post-tensioned tendons

Tendon encapsulation systems are constructed from plastic or galvanised steel materials, and are classified into two main types: those where the tendon element is subsequently bonded to the surrounding concrete by internal grouting of the duct after stressing (*bonded* post-tensioning); and those where the tendon element is permanently *debonded* from the surrounding concrete, usually by means of a greased sheath over the tendon strands (*unbonded* post-tensioning).<sup>[1]:26[5]:10</sup>

Casting the tendon ducts/sleeves into the concrete before any tensioning occurs allows them to be readily "profiled" to any desired shape including incorporating vertical and/or horizontal curvature. When the tendons are tensioned, this profiling results in reaction forces being imparted onto the hardened concrete,

and these can be beneficially used to counter any loadings subsequently applied to the structure.

[2]:5–6[5]:48:9–10

## Bonded post-tensioning

Bonded post-tensioning has prestressing tendons permanently bonded to the surrounding concrete by the *in situ* grouting of their encapsulating ducting following tendon tensioning. This grouting is undertaken for three main purposes: to protect the tendons against corrosion; to permanently "lock-in" the tendon pre-tension, thereby removing the long-term reliance upon the end-anchorage systems; and to improve certain structural behaviours of the final concrete structure.<sup>[9]</sup>

Bonded post-tensioning characteristically uses tendons each comprising *bundles* of elements (e.g. strands or wires) placed inside a single tendon duct, with the exception of bars which are mostly used unbundled. This bundling make for more efficient tendon installation and grouting processes, since each complete tendon requires only one set of end-anchorages and one grouting operation. Ducting is fabricated from a durable and corrosion-resistant material such as plastic (e.g. polyethylene) or galvanised steel, and can be either round or rectangular/oval in cross-section.<sup>[2]:7</sup> The tendon sizes used are highly dependent upon the application, ranging from building works typically using between 2-strands and 6-strands per tendon, to specialised dam works using up to 91-strands per tendon.



Multistrand post-tensioning anchor.

Fabrication of bonded tendons is generally undertaken on-site, commencing with the fitting of end-anchorages to formwork, placing the tendon ducting to the required curvature profiles, and reeving (or threading) the strands or wires through the ducting. Following concreting and tensioning, the ducts are pressure-grouted and the tendon stressing-ends sealed against corrosion.<sup>[5]:2</sup>

## Unbonded post-tensioning

Unbonded post-tensioning differs from bonded post-tensioning by allowing the tendons permanent freedom of longitudinal movement relative to the concrete. This is most commonly achieved by encasing each individual tendon element within a plastic sheathing filled with a corrosion-inhibiting grease, usually lithium based. Anchorages at each end of the tendon transfer the tensioning force to the concrete, and are required to reliably perform this role for the life of the structure.<sup>[9]:1</sup>

Unbonded post-tensioning can take the form of:

- Individual strand tendons placed directly into the concreted structure (e.g. buildings, ground slabs), or
- Bundled strands, individually greased-and-sheathed, forming a single tendon within an encapsulating duct that is placed either within or adjacent to the concrete (e.g. restressable anchors, external post-tensioning)

For individual strand tendons, no additional tendon ducting is used and no post-stressing grouting operation is required, unlike for bonded post-tensioning. Permanent corrosion protection of the strands is provided by the combined layers of grease, plastic sheathing, and surrounding concrete. Where strands are bundled to form a single unbonded tendon, an enveloping duct of plastic or galvanised steel is used and its interior free-spaces grouted after stressing. In this way, additional corrosion protection is provided via the grease, plastic sheathing, grout, external sheathing, and surrounding concrete layers.<sup>[9]:1</sup>

Individually greased-and-sheathed tendons are mostly fabricated off-site by an extrusion process. The bare steel strand is fed into a greasing chamber and then passed to an extrusion unit where molten plastic forms a continuous outer coating. Finished strands can be cut-to-length and fitted with "dead-end" anchor assemblies as required for the project.

## Comparison between bonded and unbonded post-tensioning

Both bonded and unbonded post-tensioning technologies are widely used around the world, and the choice of system to use is often dictated by regional preferences, contractor experience, or the availability of alternative systems. Either one is capable of delivering code-compliant, durable structures meeting the structural strength and serviceability requirements of the designer.<sup>[9]:2</sup>

The benefits that bonded post-tensioning can offer over unbonded systems are:

- Reduced reliance on end-anchorage integrity  
Following tensioning and grouting, bonded tendons are connected to the surrounding concrete along their full length by high-strength grout. Once cured, this grout can transfer the full tendon tension force to the concrete within a very short distance (approximately 1 metre). As a result, any



Unbonded slab post-tensioning. Installed strands and edge-anchors are visible, along with prefabricated coiled strands for the next pour



Unbonded slab post-tensioning. End-view of slab after stripping, showing individual strands and stressing-anchor recesses

inadvertent severing of the tendon or failure of an end anchorage has only a very localised impact on tendon performance, and almost never results in tendon ejection from the anchorage.<sup>[2]:18[9]:7</sup>

- **Increased ultimate strength in flexure**  
With bonded post-tensioning, any flexure of the structure gets directly resisted by tendon strains at that same location (i.e. no strain re-distribution occurs). This results in significantly higher tensile strains in the tendons than if they were unbonded, allowing their full yield strength to be realised, and producing a higher ultimate load capacity.<sup>[2]:16–17[5]:10</sup>
- **Improved crack-control**  
In the presence of concrete cracking, bonded tendons respond similarly to conventional reinforcement (rebar). With the tendons fixed to the concrete at each side of the crack, greater crack-expansion resistance is offered than with unbonded tendons, allowing many design codes to specify reduced reinforcement requirements for unbonded post-tensioning.<sup>[9]:4[10]:1</sup>
- **Improved fire performance**  
The absence of strain redistribution in bonded tendons may limit the impact that any localised overheating has on the overall structure. As a result, bonded structures may display a higher capacity to resist fire conditions than unbonded ones.<sup>[11]</sup>

The benefits that unbonded post-tensioning can offer over bonded systems are:

- **Ability to be prefabricated**  
Unbonded tendons can be readily prefabricated off-site complete with end-anchorage, facilitating faster installation during construction. Additional lead time may need to be allowed for this fabrication process.
- **Improved site productivity**  
The elimination of the post-stressing grouting process required in bonded structures improves the site-labour productivity of unbonded post-tensioning.<sup>[9]:5</sup>
- **Improved installation flexibility**  
Unbonded single-strand tendons have greater handling flexibility than bonded ducting during installation, allowing them a greater ability to be deviated around service penetrations or obstructions.<sup>[9]:5</sup>
- **Reduced concrete cover**  
Unbonded tendons may allow some reduction in concrete element thickness, as their smaller size and increased corrosion protection compared to ducted tendons may allow them to be placed closer to the concrete surface.<sup>[2]:8</sup>
- **Simpler replacement and/or adjustment**  
Being permanently isolated from the concrete, unbonded tendons are able to be readily de-stressed, re-stressed and/or replaced should they become damaged or need their force levels to be modified in-service.<sup>[9]:6</sup>
- **Superior overload performance**  
Although having a lower ultimate strength than bonded tendons, unbonded tendons' ability to redistribute strains over their full length can give them superior pre-collapse ductility. In extremis, unbonded tendons can resort to a *catenary*-type action instead of pure flexure, allowing significantly greater deformation before structural failure.<sup>[12]</sup>

## Tendon durability and corrosion protection

Long-term durability is an essential requirement for prestressed concrete given its significance as a ubiquitous, modern construction material. Research on the durability performance of in-service prestressed structures has been undertaken since the 1960s,<sup>[13]</sup> and anti-corrosion technologies for tendon protection have been continually improved since the earliest systems were developed.<sup>[14]</sup>

The durability of prestressed concrete is principally determined by the level of corrosion protection provided to any high-strength steel elements within the prestressing tendons. Also critical is the protection afforded to the end-anchorage assemblies of unbonded tendons or cable-stay systems, as the anchorages of both of these are required to retain the prestressing forces permanently. Failure of any of these components can result in the release of prestressing forces, or the physical rupture of stressing tendons.

Modern prestressing systems deliver long-term durability by addressing the following areas:

- **Tendon grouting** (bonded tendons)  
Bonded tendons consist of bundled high-strength (steel) strands placed inside ducts located within the surrounding concrete. To ensure full protection to these strands, the ducts must be pressure-filled with a corrosion-inhibiting grout, without leaving any voids, following strand-tensioning.
- **Tendon coating** (unbonded tendons)  
Unbonded tendons comprise individual high-strength strands coated in an anti-corrosion grease or wax, and fitted with a durable plastic-based full-length sleeve or sheath. The sleeving is required to be undamaged over the tendon length, and it must extend fully into the anchorage fittings at each end of the tendon.
- **Double-layer encapsulation**  
Prestressing tendons requiring permanent monitoring and/or force adjustment, such as stay-cables and re-stressable dam anchors, will typically employ double-layer corrosion protection. Such tendons are composed of individual strands, grease-coated and sleeved, collected into a strand-bundle and placed inside encapsulating polyethylene outer ducting. The remaining void space within the duct is pressure-grouted, providing a multi-layer polythene-grout-plastic-grease protection barrier system for each strand.
- **Anchorage protection**  
In all post-tensioned installations, protection of the end-anchorages against corrosion is essential, and critically so for unbonded systems

Several durability-related historical events are listed below:

- Ynys-y-Gwas bridge, West Glamorgan, Wales 1985  
A single-span, precast-segmental structure constructed in 1953 with longitudinal and transverse post-tensioning. Corrosion attacked the under-protected tendons where they crossed the *in-situ* joints between the segments, leading to sudden collapse.<sup>[14]:40</sup>
- Scheldt River bridge, Melle, Belgium 1991  
A 3-span prestressed cantilever structure constructed in the 1950s. Inadequate concrete cover in the side abutments resulted in tie-down cable corrosion, leading to a progressive failure of the main bridge span and the death of one person.<sup>[15]</sup>
- UK Highways Agency 1992  
Following discovery of tendon corrosion in several bridges in England, the Highways Agency issued a moratorium on the construction of new internally- grouted post-tensioned bridges and

embarked on a 5-year programme of inspections on its existing post-tensioned bridge stock. The moratorium was lifted in 1996.<sup>[16][17]</sup>

- Pedestrian bridge, Charlotte Motor Speedway, North Carolina, US 2000  
A multi-span steel and concrete structure constructed in 1995. An unauthorised chemical was added to the tendon grout to speed construction, leading to corrosion of the prestressing strands and the sudden collapse of one span, injuring many spectators.<sup>[18]</sup>
- Hammersmith Flyover London, England 2011  
Sixteen span prestressed structure constructed in 1961. Corrosion from road de-icing salts was detected in some of the prestressing tendons, necessitating initial closure of the road while additional investigations were done. Subsequent repairs and strengthening using external post-tensioning was carried out and completed in 2015.<sup>[19][20]</sup>

## Applications

Prestressed concrete is a highly versatile construction material as a result of it being an almost ideal combination of its two main constituents: high-strength steel, pre-stretched to allow its full strength to be easily realised; and modern concrete, pre-compressed to minimise cracking under tensile forces.<sup>[1]:12</sup> Its wide range of application is reflected in its incorporation into the major design codes covering most areas of structural and civil engineering, including buildings, bridges, dams, foundations, pavements, piles, stadiums, silos, and tanks.<sup>[6]</sup>

### Building structures

Building structures are typically required to satisfy a broad range of structural, aesthetic and economic requirements. Significant among these include: a minimum number of (intrusive) supporting walls or columns; low structural thickness (depth), allowing space for services, or for additional floors in high-rise construction; fast construction cycles, especially for multi-storey buildings; and a low cost-per-unit-area, to maximise the building owner's return on investment.

The prestressing of concrete allows "load-balancing" forces to be introduced into the structure to counter the loadings which will apply in-service. This provides many benefits to building structures:

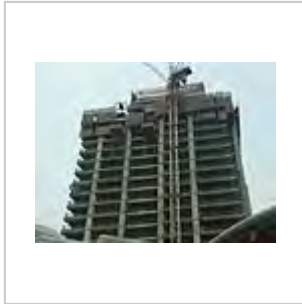
- Longer spans for the same structural depth  
Load-balancing results in lower in-service deflections, which allows spans to be increased (and the number of supports reduced) without adding to structural depth.
- Reduced structural thickness  
For a given span, lower in-service deflections allows thinner structural sections to be used, in turn resulting in lower floor-to-floor heights, or more room for building services.
- Faster stripping time  
Typically, prestressed concrete building elements are fully stressed and self-supporting within five days. At this point they can have their formwork stripped and re-deployed to the next section of the building, accelerating construction "cycle-times".
- Reduced material costs  
The combination of reduced structural thickness, reduced conventional reinforcement quantities, and fast construction often results in prestressed concrete showing significant cost benefits in building structures compared to alternative structural materials.



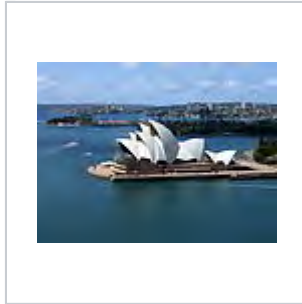
Some notable building structures constructed from prestressed concrete include: Sydney Opera House,<sup>[21]</sup> St George Wharf Tower, London,<sup>[22]</sup> CN Tower, Toronto,<sup>[23]</sup> Kai Tak Cruise Terminal, Hong Kong,<sup>[24]</sup> Ocean Heights 2, Dubai,<sup>[25]</sup> World Tower, Sydney,<sup>[26]</sup> Eureka Tower, Melbourne<sup>[27]</sup> Torre Espacio, Madrid,<sup>[28]</sup> Guoco Tower (Tanjong Pagar Centre), Singapore,<sup>[29]</sup> Zagreb International Airport, Croatia,<sup>[30]</sup> Capital Gate, Abu Dhabi UAE,<sup>[31]</sup> International Commerce Centre, Hong Kong.<sup>[32]</sup>



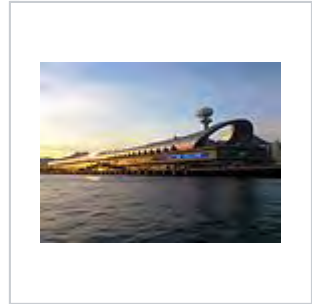
ICC tower, Hong Kong  
484m 2010



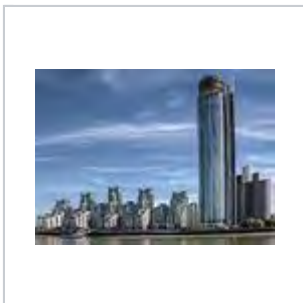
Guoco Tower,  
Singapore  
290m 2016



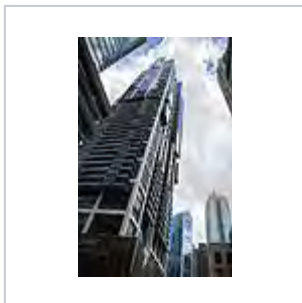
Sydney Opera House  
1973



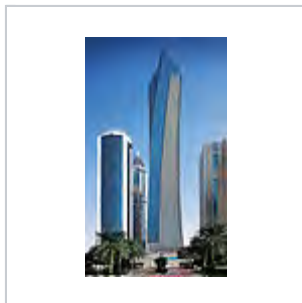
Kai Tak Terminal  
Hong Kong 2013



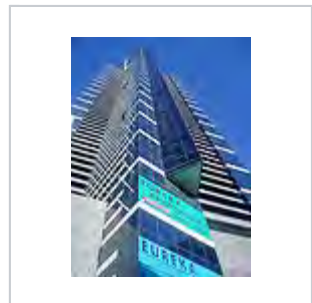
St George Wharf,  
London  
181m 2014



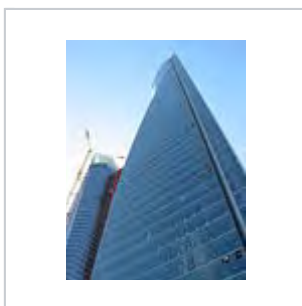
World Tower, Sydney  
230m 2004



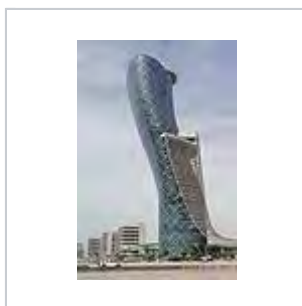
Ocean Heights 2, Dubai  
335m 2016



Eureka Tower,  
Melbourne  
297m 2006



Torre Espacio, Madrid  
230m 2008



Capital Gate, Abu  
Dhabi  
18° lean 2010

## Civil structures

### Bridges

Of the wide range of alternative methods and materials that are available for the construction of bridges, concrete remains the most popular structural material, and prestressed concrete in particular is frequently adopted.<sup>[33][34]</sup>

In short-span bridges (~10-40m spans), prestressing is commonly employed in the form of precast pre-tensioned girders or planks;<sup>[35]</sup> for medium-length structures (~40m-200m spans), precast-segmental, *in-situ* balanced-cantilever and incrementally-launched designs are all efficiently constructed using prestressing;<sup>[36]</sup> while for the longest bridges, prestressed concrete deck structures often form an integral part of cable-stayed designs.<sup>[37]</sup>

### Dams

Concrete dams have used prestressing to counter uplift and increase their overall stability since the mid 1930s.<sup>[38][39]</sup> Prestressing is also frequently retro-fitted as part of dam remediation works, such as for structural strengthening, or when raising crest or spillway heights.<sup>[40][41]</sup>

Most commonly, dam prestressing takes the form of post-tensioned anchors drilled into the dam's concrete structure and/or the underlying rock strata. Such anchors typically comprise tendons of high-tensile bundled steel strands or individual threaded bars. Tendons are grouted to the concrete or rock at their far (internal) end, and have a significant "de-bonded" free-length at their external end which allows the tendon to stretch during tensioning. Tendons may be full-length bonded to the surrounding concrete or rock once tensioned, or (more commonly) have strands permanently encapsulated in corrosion-inhibiting grease over the free-length to permit long-term load monitoring and re-stressability.<sup>[42]</sup>

### Silos and tanks

Circular storage structures such as silos and tanks can use prestressing forces to directly resist the outward pressures generated by stored liquids or bulk-solids. Horizontally curved tendons are installed within the concrete wall to form a series of "hoops" spaced vertically up the structure. When tensioned, these tendons exert both axial (compressive) and radial (inward) forces onto the structure, which can be used to directly oppose the subsequent storage loadings. If the magnitude of the prestress is designed to always exceed the tensile stresses produced by the loadings, a permanent residual compression will exist in the wall concrete, assisting in maintaining a watertight, crack-free structure under all storage conditions.<sup>[43][44][45][46]:61</sup>

### Nuclear and blast-containment structures

Prestressed concrete is long-established as a reliable construction material for high-pressure containment structures such as nuclear reactor vessels and containment buildings, and petrochemical tank blast-containment walls. Using prestressing to place such structures into an initial state of bi-axial or tri-axial compression increases their resistance to concrete cracking and leakage, while providing a proof-loaded, redundant and monitorable pressure-containment system.<sup>[47]:585–594</sup><sup>[48]</sup><sup>[49]</sup>

Nuclear reactor and containment vessels will commonly employ separate sets of post tensioned tendons curved horizontally or vertically to completely envelop the reactor core, while blast containment walls for LNG tanks and similar will normally utilise layers of horizontally-curved hoop tendons for containment in combination with vertically looped tendons for axial wall prestressing.

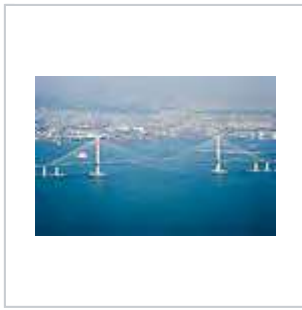
### **Hardstands and pavements**

Heavily loaded concrete ground-slabs and pavements can be sensitive to cracking and subsequent traffic-driven deterioration. As a result, prestressed concrete is regularly used in such structures as its pre-compression provides the concrete with the ability to resist the crack-inducing tensile stresses generated by in-service loading. This crack-resistance also allows individual slab sections to be constructed in larger pours than for conventionally reinforced concrete, resulting in wider joint spacings, reduced jointing costs and less long-term joint maintenance issues.<sup>[47]:594–598</sup><sup>[50]</sup> Initial works have also been successfully conducted on the use of precast prestressed concrete for road pavements, where the speed and quality of the construction has been noted as being beneficial for this technique.<sup>[51]</sup>

Some notable civil structures constructed using prestressed concrete include: Gateway Bridge, Brisbane Australia,<sup>[52]</sup> Incheon Bridge South Korea,<sup>[53]</sup> Roseires Dam Sudan,<sup>[54]</sup> Wanapum Dam Washington US,<sup>[55]</sup> LNG tanks, South Hook Wales, Cement silos, Brevik Norway, Autobahn A73 bridge, Itz Valley Germany, Ostankino Tower, Moscow Russia, CN Tower, Toronto Canada, Ringhals nuclear reactor Videbergshamn Sweden<sup>[48]:37</sup>



Gateway Bridge  
Brisbane, Aust.



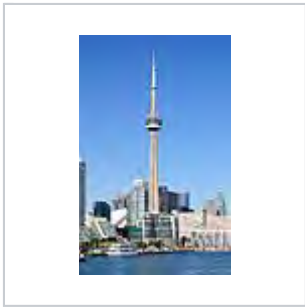
Incheon Bridge  
South Korea



Autobahn A73  
Itz Valley, Germany



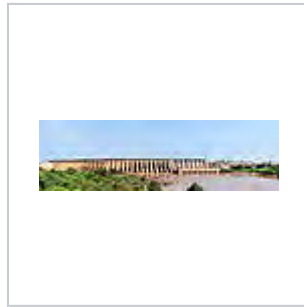
Ostankino Tower  
Moscow, Russia



CN Tower  
Toronto, Canada



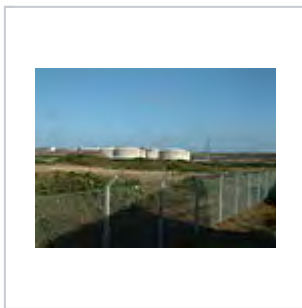
Norcem silos  
Brevik, Norway



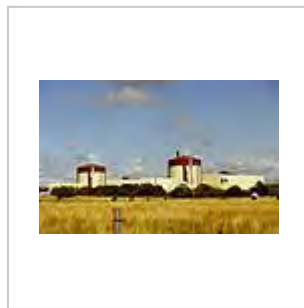
Roseires Dam  
Ad Damazin, Sudan



Wanapum Dam  
Washington, US



LNG tanks  
South Hook, Wales



Ringhals nuclear plant  
Videbergshamn,  
Sweden

## Design agencies and regulations

Worldwide, many professional organizations exist to promote best practice in the design and construction of prestressed concrete structures. In the United States, such organizations include the Post-Tensioning Institute (PTI) and the Precast/Prestressed Concrete Institute (PCI (<http://www.pci.org/>)). Similar bodies include the Canadian Precast/Prestressed Concrete Institute (CPCI (<http://www.cpci.ca/>)), the UK's Post-Tensioning Association (<http://www.posttensioning.co.uk/>), the Post Tensioning Institute of Australia (<http://www.ptia.org.au/>) and the South African Post Tensioning Association (<http://www.sapta.co.za/>). Europe has similar country-based associations and institutions.

It is important to note that these organizations are not the authorities of building codes or standards, but rather exist to promote the understanding and development of prestressed concrete design, codes and best practices.

Rules and requirements for the detailing of reinforcement and prestressing tendons are specified by individual national codes and Standards such as the European Standard EN 1992-2:2005 – Eurocode 2: Design of Concrete Structures, the US Standard ACI318: Building Code Requirements for Reinforced Concrete, and the Australian Standard AS 3600-2009: Concrete Structures.

## See also

- Box girder bridge
- Cable stayed bridge
- Concrete
- Concrete slab
- Dyckerhoff & Widmann AG (Dywidag)
- Eugène Freyssinet
- Glossary of prestressed concrete terms
- Hollow-core slab
- Precast concrete
- Prestressed structure
- Properties of concrete
- Reinforced concrete
- Reinforcing bar
- Segmental bridge



Wikimedia Commons has media related to ***Prestressed concrete***.

## References

1. Lin, T.Y.; Burns, Ned H. (1981). *Design of Prestressed Concrete Structures* (Third ed.). New York, US: John Wiley & Sons. ISBN 0 471 01898 8.
2. Federation Internationale du Beton (Feb 2005). *fib Bulletin 31: Post-tensioning in Buildings* (PDF). FIB. ISBN 978 2 88394 071 0. Retrieved 26 August 2016.
3. American Concrete Institute. "CT-13: ACI Concrete Terminology". *American Concrete Institute*. Farmington Hills, Michigan US: ACI. Retrieved 25 August 2016.
4. Warner, R. F.; Rangan, B. V.; Hall, A. S.; Faulkes, K. A. (1988). *Concrete Structures*. South Melbourne, Australia: Addison Welsley Longman. pp. 8–19. ISBN 0 582 80247 4.
5. Warner, R. F.; Faulkes, K. A. (1988). *Prestressed Concrete* (2nd ed.). Melbourne, Australia: Longman Cheshire. pp. 1–13. ISBN 0 582 71225 4.
6. Post-Tensioning Institute (2006). *Post-Tensioning Manual* (6th ed.). Phoenix, AZ US: PTI. pp. 5–54. ISBN 0 9778752 0 2.
7. Tokyo Rope Mfg Co Ltd. "CFCC Pre-tensioning Manual" (PDF). *MaineDOT*. Retrieved 19 August 2016.
8. "Tendons having one or more deviations from a straight line, either vertically or horizontally, between the ends of the structure"
9. Aalami, Bijan O. (5 September 1994). "Unbonded and bonded post-tensioning systems in building construction" (PDF). *PTI Technical Notes*. Phoenix, Arizona US: Post-Tensioning Institute (5). Retrieved 23 August 2016.
10. Aalami, Bijan O. (February 2001). "Nonprestressed Bonded Reinforcement in Post-Tensioned Building Design" (PDF). *ADAPT Technical Publication* (P2-01). Retrieved 25 August 2016.

11. Bailey, Colin G.; Ellobody, Ehab (2009). "Comparison of unbonded and bonded post-tensioned concrete slabs under fire conditions". *The Structural Engineer*. **87** (19). Retrieved 22 August 2016.
12. Bondy, Kenneth B. (December 2012). "Tow way post-tensioned slabs with bonded tendons" (PDF). *PTI Journal*. US: Post-Tensioning Institute. **8** (2): 44. Retrieved 25 August 2016.
13. Szilard, Rudolph (October 1969). "Survey on the Durability of Prestressed Concrete Structures" (PDF). *PCI Journal*: 62–73. Retrieved 7 September 2016.
14. Podolny, Walter (September 1992). "Corrosion of Prestressing Steels and its Mitigation" (PDF). *PCI Journal*: 34–55. Retrieved 7 September 2016.
15. De Schutter, Geert (10 May 2012). *Damage to Concrete Structures*. CRC Press. pp. 31–33. ISBN 9780415603881. Retrieved 7 September 2016.
16. Ryall, M. J.; Woodward, R.; Milne, D. (2000). *Bridge Management 4: Inspection, Maintenance, Assessment and Repair*. London: Thomas Telford. pp. 170–173. Retrieved 7 September 2016.
17. CARES. "Post-Tensioning Systems". *www.ukcares.com*. CARES. Retrieved 7 September 2016.
18. NACE. "Corrosion Failures: Lowe's Motor Speedway Bridge Collapse". *www.nace.org*. NACE. Retrieved 7 September 2016.
19. Ed Davey and Rebecca Cafe (3 December 2012). "TfL report warned of Hammersmith Flyover collapse risk". BBC News, London. Retrieved 3 December 2012.
20. Freyssinet. "Extending the Life of Hammersmith Flyover". *www.freyssinet.com*. Freyssinet. Retrieved 7 September 2016.
21. Australian Society for History of Engineering and Technology. "An Engineering Walk around the Sydney Opera House" (PDF). *ashet.org.au*. ASHET. Retrieved 1 September 2016.
22. "The Tower, One St. George Wharf, London, UK". *cclint.com*. CCL. Retrieved 1 September 2016.
23. Knoll, Franz; Prosser, M. John; Otter, John (May–June 1976). "Prestressing the CN Tower" (PDF). *PCI Journal*: 84–111.
24. VSL. "Kai Tak Cruise Terminal Building - Hong Kong" (PDF). *vslvietnam.com*. VSL. Retrieved 1 September 2016.
25. CM Engineering Consultants. "Ocean Heights 2, Dubai UAE". *http://www.cmeecs.co*. CMECS. Retrieved 1 September 2016. External link in `|website=` (help)
26. Martin, Owen; Lal, Nalean. "Structural Design of the 84 Storey World Tower in Sydney" (PDF). *ctbuh.org*. Council on Tall Buildings and Urban Habitat. Retrieved 1 September 2016.
27. Design Build Network. "Eureka Tower, Melbourne Victoria Australia". *http://www.designbuild-network.com/*. Design Build Network. Retrieved 1 September 2016. External link in `|website=` (help)
28. Martinez, Julio; Gomez, Miguel (July 2008). "Torre Espacio. Building Structure". *Hormigon y Acero*. Madrid, Spain. **59** (249): 19–43. ISSN 0439-5689. Retrieved 1 September 2016.
29. BBR Network (2016). "Reaching for the Skies" (PDF). *Connaect*. **10**: 51. Retrieved 2 September 2016.
30. BBR Network (2016). "Gateway to South Eastern Europe" (PDF). *Connaect*. **10**: 37–41.
31. Schofield, Jeff (2012). "Case Study: Capital Gate, Abu Dhabi" (PDF). *CTBUH Journal* (11). Retrieved 2 September 2016.
32. ARUP. "International Commerce Centre (ICC)". *www.arup.com*. ARUP. Retrieved 2 September 2016.
33. Man-Chung, Tang (2007). "Evolution of Bridge Technology" (PDF). *IABSE Symposium Proceedings: 7*. Retrieved 5 September 2016.
34. Hewson, Nigel R. (2012). *Prestressed Concrete bridges: design and Construction*. ICE. ISBN 9780727741134. Retrieved 2 September 2016.
35. Main Roads Western Australia. "Structures Engineering Design Manual" (PDF). *www.mainroads.wa.gov.au*. MRWA. pp. 17–23. Retrieved 2 September 2016.
36. LaViolette, Mike (December 2007). *Bridge Construction Practices Using Incremental Launching* (PDF). AASHTO. p. Appendix A.
37. Leonhardt, Fritz (September 1987). "Cable Stayed Bridges with Prestressed Concrete". *PCI Journal*: 52–80.
38. Roemermann, A. C. (February 1965). "Prestressed Concrete Dams: 1936-1964" (PDF). *PCI Journal*: 76–88. Retrieved 2 September 2016.
39. Brown, E. T. (February 2015). "Rock-engineering design of post-tensioned anchors for dams - A review". *Journal of Rock Mechanics and Geological Engineering*. **7** (1): 1–13. Retrieved 6 September 2016.
40. Institution of Engineers Australia. "Catagunya Dam Tasmania" (PDF). *www.engineersaustralia.org.au*. IEAust. Retrieved 2 September 2016.

41. Xu, Haixue; Benmokrane, Brahim (1996). "Strengthening of existing concrete dams using post-tensioned anchors: A state-of-the-art review". *Canadian Journal of Civil Engineering*. **23** (6): 1151–1171. Retrieved 2 September 2016.
42. Cavill, Brian (20 March 1997). "Very High capacity Ground Anchors Used in Strengthening Concrete Gravity Dams". *Conference Proceedings*. London UK: Institution of Civil Engineers: 262.
43. Priestley, M. J. N. (July 1985). "Analysis and Design of Prestressed Circular Concrete Storage Tanks" (PDF). *PCI Journal*: 64–85. Retrieved 5 September 2016.
44. Ghali, Amin (12 May 2014). *Circular Storage Tanks and Silos* (Third ed.). CRC Press. pp. 149–165. ISBN 9781466571044. Retrieved 5 September 2016.
45. "Circular Prestressing". *theconstructor.org*. The Constructor.org. Retrieved 5 September 2016.
46. Gilbert, R. I.; Mickleborough, N. C.; Ranzi, G. (17 Feb 2016). *Design of Prestressed Concrete to AS3600-2009* (Second ed.). CRC Press. Retrieved 5 September 2016.
47. Raju, Krishna. *Prestressed Concrete* (PDF) (Fourth ed.). New Delhi: Tata McGraw Hill. ISBN 0 07 063444 0. Retrieved 5 September 2016.
48. Bangash, M. Y. H. (2011). *Structures for Nuclear Facilities - Analysis, Design and Construction*. London: Springer. pp. 36–37. ISBN 978 3 642 12560 7. Retrieved 5 September 2016.
49. Gerwick, Ben C. (13 Feb 1997). *Construction of Prestressed Concrete Structures* (Second ed.). New York: John Wiley & Sons. pp. 472–494. ISBN 0 471 53915 5. Retrieved 5 September 2016.
50. "Building Post-Tensioned Slabs on Grade". *www.concreteconstruction.net*. Concrete Construction. Retrieved 5 September 2016.
51. Merritt, David; Rogers, Richard; Rasmussen, Robert (March 2008). *Construction of a Precast Prestressed Concrete Pavement Demonstration Project on Interstate 57 near Sikeston, Missouri* (PDF). US DOT Federal Highway Administration. Retrieved 5 September 2016.
52. Connall, John; Wheeler, Paul; Pau, Andrew; Mihov, Miho. "Design of the Main Spans, Second Gateway Bridge, Brisbane" (PDF). *www.cmnzl.co.nz*. Retrieved 2 September 2016.
53. DYWIDAG. "Incheon Bridge, Seoul, South Korea". *www.dywidag-systems.a*. DYWIDAG. Retrieved 2 September 2016.
54. "SRG Remote Projects" (PDF). *www.srglimited.com.au*. SRG Limited. p. 10. Retrieved 6 September 2016.
55. Eberhardt, A.; Veltrop, J. A. (August 1965). "1300-Ton-Capacity Prestressed Anchors Stabilize Dam" (PDF). *PCI Journal*: 18–43. Retrieved 6 September 2016.

## External links

- The story of prestressed concrete from 1930 to 1945: A step towards the European Union ([http://www.sedhc.es/biblioteca/actas/CIHC1\\_130\\_Marrey%20B.pdf](http://www.sedhc.es/biblioteca/actas/CIHC1_130_Marrey%20B.pdf))
- Guidelines for Sampling, Assessing, and Restoring Defective Grout in Prestressed Concrete Bridge Post-Tensioning Ducts (<http://purl.fdlp.gov/GPO/gpo41564>) Federal Highway Administration
- Historical Patents and the Evolution of Twentieth Century Architectural Construction with Reinforced and Pre-stressed Concrete (<http://www.arct.cam.ac.uk/Downloads/ichs/vol-2-1719-1740-anaya.pdf>)

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