

Wind turbine design

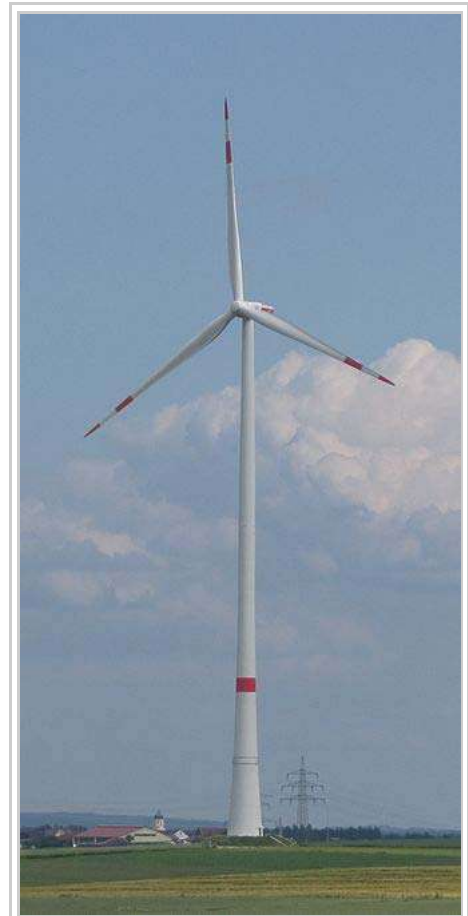
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Wind turbine design is the process of defining the form and specifications of a wind turbine to extract energy from the wind.^[1] A wind turbine installation consists of the necessary systems needed to capture the wind's energy, point the turbine into the wind, convert mechanical rotation into electrical power, and other systems to start, stop, and control the turbine.

This article covers the design of horizontal axis wind turbines (HAWT) since the majority of commercial turbines use this design.

In 1919 the physicist Albert Betz showed that for a hypothetical ideal wind-energy extraction machine, the fundamental laws of conservation of mass and energy allowed no more than $16/27$ (59.3%) of the kinetic energy of the wind to be captured. This Betz' law limit can be approached by modern turbine designs which may reach 70 to 80% of this theoretical limit.

In addition to aerodynamic design of the blades, design of a complete wind power system must also address design of the hub, controls, generator, supporting structure and foundation. Further design questions arise when integrating wind turbines into electrical power grids.



An example of a wind turbine, this 3 bladed turbine is the classic design of modern wind turbines

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Aerodynamics

The shape and dimensions of the blades of the wind turbine are determined by the aerodynamic performance required to efficiently extract energy from the wind, and by the strength required to resist the forces on the blade.

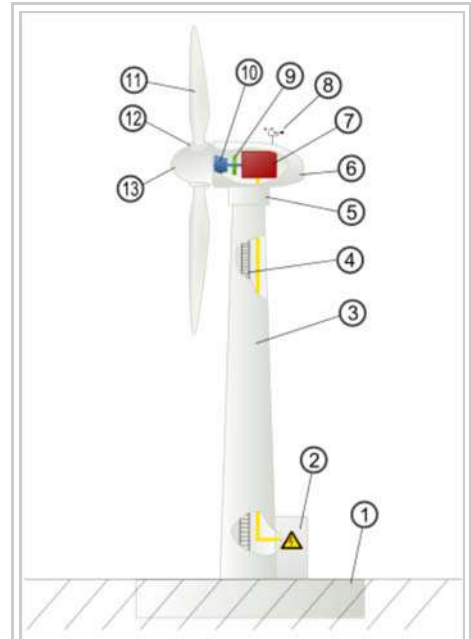
The aerodynamics of a horizontal-axis wind turbine are not straightforward. The air flow at the blades is not the same as the airflow far away from the turbine. The very nature of the way in which energy is extracted from the air also causes air to be deflected by the turbine. In addition the aerodynamics of a wind turbine at the rotor surface exhibit phenomena that are rarely seen in other aerodynamic fields.

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Power control

The speed at which a wind turbine rotates must be controlled for efficient power generation and to keep the turbine components within designed speed and torque limits. The centrifugal force on the spinning blades increases as the square of the rotation speed, which makes this structure sensitive to overspeed. Because the power of the wind increases as the cube of the wind speed, turbines have to be built to survive much higher wind loads (such as gusts of wind) than those from which they can practically generate power. Wind turbines have ways of reducing torque in high winds.

A wind turbine is designed to produce power over a range of wind speeds. All wind turbines are designed for a maximum wind speed, called the survival speed, above which they will be damaged. The survival speed of



Wind turbine components :

1-Foundation, 2-Connection to the electric grid, 3-Tower, 4-Access ladder, 5-Wind orientation control (Yaw control), 6-Nacelle, 7-Generator, 8-Anemometer, 9-Electric or Mechanical Brake, 10-Gearbox, 11-Rotor blade, 12-Blade pitch control, 13-Rotor hub.



Wind rotor profile

commercial wind turbines is in the range of 40 m/s (144 km/h, 89 MPH) to 72 m/s (259 km/h, 161 MPH). The most common survival speed is 60 m/s (216 km/h, 134 MPH).

If the rated wind speed is exceeded the power has to be limited. There are various ways to achieve this.

A control system involves three basic elements: sensors to measure process variables, actuators to manipulate energy capture and component loading, and control algorithms to coordinate the actuators based on information gathered by the sensors.^[2]

Stall

Stalling works by increasing the angle at which the relative wind strikes the blades (angle of attack), and it reduces the induced drag (drag associated with lift). Stalling is simple because it can be made to happen passively (it increases automatically when the winds speed up), but it increases the cross-section of the blade face-on to the wind, and thus the ordinary drag. A fully stalled turbine blade, when stopped, has the flat side of the blade facing directly into the wind.

A fixed-speed HAWT (Horizontal Axis Wind Turbine) inherently increases its angle of attack at higher wind speed as the blades speed up. A natural strategy, then, is to allow the blade to stall when the wind speed increases. This technique was successfully used on many early HAWTs. However, on some of these blade sets, it was observed that the degree of blade pitch tended to increase audible noise levels.

Vortex generators may be used to control the lift characteristics of the blade. The VGs are placed on the airfoil to enhance the lift if they are placed on the lower (flatter) surface or limit the maximum lift if placed on the upper (higher camber) surface.^[3]

Furling works by decreasing the angle of attack, which reduces the induced drag from the lift of the rotor, as well as the cross-section. One major problem in designing wind turbines is getting the blades to stall or furl quickly enough should a gust of wind cause sudden acceleration. A fully furled turbine blade, when stopped, has the edge of the blade facing into the wind.

Loads can be reduced by making a structural system softer or more flexible.^[2] This could be accomplished with downwind rotors or with curved blades that twist naturally to reduce angle of attack at higher wind speeds. These systems will be nonlinear and will couple the structure to the flow field - thus, design tools must evolve to model these nonlinearities.

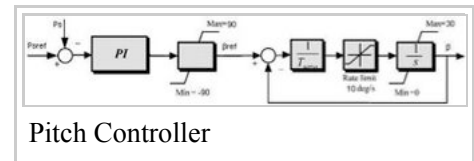
Standard modern turbines all furl the blades in high winds. Since furling requires acting against the torque on the blade, it requires some form of pitch angle control, which is achieved with a slewing drive. This drive precisely angles the blade while withstanding high torque loads. In addition, many turbines use hydraulic systems. These systems are usually spring-loaded, so that if hydraulic power fails, the blades automatically furl. Other turbines use an electric servomotor for every rotor blade. They have a small battery-reserve in case of an electric-grid breakdown. Small wind turbines (under 50 kW) with variable-pitching generally use systems operated by centrifugal force, either by flyweights or geometric design, and employ no electric or hydraulic controls.

Fundamental gaps exist in pitch control, limiting the reduction of energy costs, according to a report from a coalition of researchers from universities, industry, and government, supported by the Atkinson Center for a Sustainable Future. Load reduction is currently focused on full-span blade pitch control, since individual pitch motors are the actuators currently available on commercial turbines. Significant load mitigation has been demonstrated in simulations for blades, tower, and drive train. However, there is still research needed, the

methods for realization of full-span blade pitch control need to be developed in order to increase energy capture and mitigate fatigue loads.

A control technique applied to the pitch angle is done by comparing the current active power of the engine with the value of active power at the rated engine speed (active power reference, P_s reference). Control of the pitch angle in this case is done with a PI controller controls. However, in order to have a realistic response to the control system of the pitch angle, the actuator uses the time constant T_{servo} , an integrator and limiters so as the pitch angle to be from 0° to 30° with a rate of change ($\pm 10^\circ$ per sec).

From the figure at the right, the reference pitch angle is compared with the actual pitch angle b and then the error is corrected by the actuator. The reference pitch angle, which comes from the PI controller, goes through a limiter. Restrictions on limits are very important to maintain the pitch angle in real term. Limiting the rate of change is very important especially during faults in the network. The importance is due to the fact that the controller decides how quickly it can reduce the aerodynamic energy to avoid acceleration during errors.



[2]

Other controls

Generator torque

Modern large wind turbines are variable-speed machines. When the wind speed is below rated, generator torque is used to control the rotor speed in order to capture as much power as possible. The most power is captured when the tip speed ratio is held constant at its optimum value (typically 6 or 7). This means that as wind speed increases, rotor speed should increase proportionally. The difference between the aerodynamic torque captured by the blades and the applied generator torque controls the rotor speed. If the generator torque is lower, the rotor accelerates, and if the generator torque is higher, the rotor slows down. Below rated wind speed, the generator torque control is active while the blade pitch is typically held at the constant angle that captures the most power, fairly flat to the wind. Above rated wind speed, the generator torque is typically held constant while the blade pitch is active.

One technique to control a permanent magnet synchronous motor is Field Oriented Control. Field Oriented Control is a closed loop strategy composed of two current controllers (an inner loop and outer loop cascade design) necessary for controlling the torque, and one speed controller.

Constant torque angle control

In this control strategy the d axis current is kept zero, while the vector current is align with the q axis in order to maintain the torque angle equal with 90° . This is one of the most used control strategy because of the simplicity, by controlling only the I_{qs} current. So, now the electromagnetic torque equation of the permanent magnet synchronous generator is simply a linear equation depend on the I_{qs} current only.

So, the electromagnetic torque for $I_{ds} = 0$ (we can achieve that with the d-axis controller) is now:

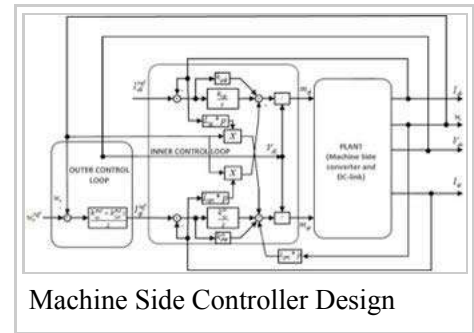
$$T_e = \frac{3}{2} p (\lambda_{pm} I_{qs} + (L_{ds} - L_{qs}) I_{ds} I_{qs}) = \frac{3}{2} p \lambda_{pm} I_{qs}$$

So, the complete system of the machine side converter and the cascaded PI controller loops is given by the

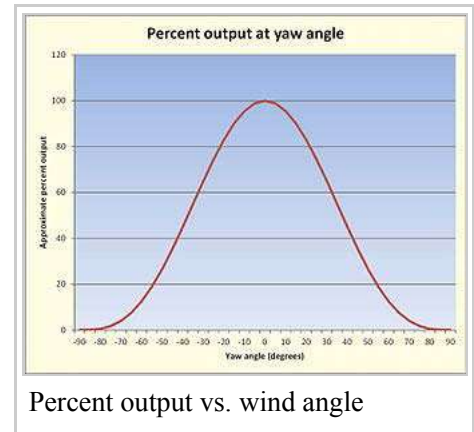
figure in the right. In that we have the control inputs, which are the duty ratios m_{ds} and m_{qs} , of the PWM-regulated converter. Also, we can see the control scheme for the wind turbine in the machine side and simultaneously how we keep the I_{ds} zero (the electromagnetic torque equation is linear).

Yawing

Modern large wind turbines are typically actively controlled to face the wind direction measured by a wind vane situated on the back of the nacelle. By minimizing the yaw angle (the misalignment between wind and turbine pointing direction), the power output is maximized and non-symmetrical loads minimized. However, since the wind direction varies quickly the turbine will not strictly follow the direction and will have a small yaw angle on average. The power output losses can simply be approximated to fall with $(\cos(\text{yaw angle}))^3$. Particularly at low-to-medium wind speeds, yawing can make a significant reduction in turbine output, with wind direction variations of $\pm 30^\circ$ being quite common and long response times of the turbines to changes in wind direction. At high wind speeds, the wind direction is less variable.



Machine Side Controller Design



Percent output vs. wind angle

Electrical braking

Braking of a small wind turbine can be done by dumping energy from the generator into a resistor bank, converting the kinetic energy of the turbine rotation into heat. This method is useful if the kinetic load on the generator is suddenly reduced or is too small to keep the turbine speed within its allowed limit.

Cyclically braking causes the blades to slow down, which increases the stalling effect, reducing the efficiency of the blades. This way, the turbine's rotation can be kept at a safe speed in faster winds while maintaining (nominal) power output. This method is usually not applied on large grid-connected wind turbines.

Mechanical braking

A mechanical drum brake or disk brake is used to stop turbine in emergency situation such as extreme gust events or over speed. This brake is a secondary means to hold the turbine at rest for maintenance, with a rotor lock system as primary means. Such brakes are usually applied only after blade furling and electromagnetic braking have reduced the turbine speed generally 1 or 2 rotor RPM, as the mechanical brakes can create a fire inside the nacelle if used to stop the turbine from full speed. The load on the turbine increases if the brake is applied at rated RPM. Mechanical brakes are driven by hydraulic systems and are connected to main control box.



2kW Dynamic braking resistor for small wind turbine.

Turbine size

There are different size classes of wind turbines. The smallest having power production less than 10 kW are used in homes, farms and remote applications whereas intermediate wind turbines (10-250 kW) are useful for village power, hybrid systems and distributed power. The largest wind turbines (660 kW – 2+MW) are used in central station wind farms, distributed power and community wind.^[4]

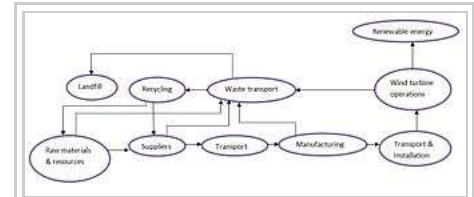


Figure 1. Flow diagram for wind turbine plant



A person standing beside 15 m long blades.

For a given survivable wind speed, the mass of a turbine is approximately proportional to the cube of its blade-length. Wind power intercepted by the turbine is proportional to the square of its blade-length.^[5] The maximum blade-length of a turbine is limited by both the strength and stiffness of its material.

Labor and maintenance costs increase only gradually with increasing turbine size, so to minimize costs, wind farm turbines are basically limited by the strength of materials, and siting requirements.

Typical modern wind turbines have diameters of 40 to 90 metres (130 to 300 ft) and are rated between 500 kW and 2 MW. As of 2014 the most powerful turbine, the Vestas V-164, is rated at 8 MW and has a rotor diameter of 164m.^[6]

Nacelle

The nacelle is housing the gearbox and generator connecting the tower and rotor. Sensors detect the wind speed and direction, and motors turn the nacelle into the wind to maximize output.

Gearbox

In conventional wind turbines, the blades spin a shaft that is connected through a gearbox to the generator. The gearbox converts the turning speed of the blades 15 to 20 rotations per minute for a large, one-megawatt turbine into the faster 1,800 rotations per minute that the generator needs to generate electricity.^[7] Analysts from GlobalData estimate that gearbox market grows from \$3.2bn in 2006 to \$6.9bn in 2011, and to \$8.1bn by 2020. Market leaders were Winergy in 2011.^[8] The use of magnetic gearboxes has also been explored as a way of reducing wind turbine maintenance costs.^[9]

Generator

For large, commercial size horizontal-axis wind turbines, the electrical generator^[10] is mounted in a nacelle at the top of a tower, behind the hub of the turbine rotor. Typically wind turbines generate electricity through asynchronous machines that are directly connected with the electricity grid. Usually the rotational speed of the wind turbine is slower than the equivalent rotation speed of the electrical network: typical rotation speeds for wind generators are 5–20 rpm while a directly connected machine will have an electrical speed between 750 and 3600 rpm. Therefore, a gearbox is inserted between the rotor hub and the generator. This also reduces the generator cost and weight. Commercial size generators have a rotor carrying a field winding so that a rotating magnetic field is produced inside a set of windings called the stator. While the rotating field winding consumes a fraction of a percent of the generator output, adjustment of the field current allows good control over the generator output voltage.

Older style wind generators rotate at a constant speed, to match power line frequency, which allowed the use of less costly induction generators. Newer wind turbines often turn at whatever speed generates electricity most efficiently. The varying output frequency and voltage can be matched to the fixed values of the grid using multiple technologies such as doubly fed induction generators or full-effect converters where the variable frequency current produced is converted to DC and then back to AC. Although such alternatives require costly equipment and cause power loss, the turbine can capture a significantly larger fraction of the wind energy. In some cases, especially when turbines are sited offshore, the DC energy will be transmitted from the turbine to a central (onshore) inverter for connection to the grid.



Gearbox, rotor shaft and brake assembly

Gearless wind turbine

Gearless wind turbines (also called direct drive) get rid of the gearbox completely. Instead, the rotor shaft is attached directly to the generator, which spins at the same speed as the blades. Enercon and EWT (formerly known as Lagerwey) have produced gearless wind turbines with separately electrically excited generators for many years,^[11] and Siemens produces a gearless "inverted generator" 3 MW model^{[12][13]} while developing a 6 MW model.^[14] To make up for a direct drive generator's slower spinning rate, the diameter of the generator's rotor is increased so that it can contain more magnets to create the required frequency and power.

Gearless wind turbines are often heavier than gear based wind turbines. A study by the EU called "Reliawind"^[15] based on the largest sample size of turbines has shown that the reliability of gearboxes is not the main problem in wind turbines. The reliability of direct drive turbines offshore is still not known, since the sample size is so small.

Experts from Technical University of Denmark estimate that a geared generator with permanent magnets may use 25 kg/MW of the rare earth element Neodymium, while a gearless may use 250 kg/MW.^[16]

In December 2011, the US Department of Energy published a report stating critical shortage of rare earth elements such as neodymium used in large quantities for permanent magnets in gearless wind turbines.^[17] China produces more than 95% of rare earth elements, while Hitachi holds more than 600 patents covering Neodymium magnets. Direct-drive turbines require 600 kg of permanent magnet material per megawatt, which translates to several hundred kilograms of rare earth content per megawatt, as neodymium content is estimated to be 31% of magnet weight. Hybrid drivetrains (intermediate between direct drive and traditional geared) use significantly less rare earth materials. While permanent magnet wind turbines only account for about 5% of the market outside of China, their market share inside of China is estimated at 25% or higher. In 2011, demand for neodymium in wind turbines was estimated to be 1/5 of that in electric vehicles.^[17]

Blades

Blade design

The ratio between the speed of the blade tips and the speed of the wind is called tip speed ratio. High efficiency 3-blade-turbines have tip speed/wind speed ratios of 6 to 7. Modern wind turbines are designed to spin at varying speeds (a consequence of their generator design, see above). Use of aluminum and composite materials in their blades has contributed to low rotational inertia, which means that newer wind turbines can accelerate

quickly if the winds pick up, keeping the tip speed ratio more nearly constant. Operating closer to their optimal tip speed ratio during energetic gusts of wind allows wind turbines to improve energy capture from sudden gusts that are typical in urban settings.

And in contrast, older style wind turbines were designed with heavier steel blades, which have higher inertia, and rotated at speeds governed by the AC frequency of the power lines. The high inertia buffered the changes in rotation speed and thus made power output more stable.

It is generally understood that noise increases with higher blade tip speeds. To increase tip speed without increasing noise would allow reduction the torque into the gearbox and generator and reduce overall structural loads, thereby reducing cost.^[2] The reduction of noise is linked to the detailed aerodynamics of the blades, especially factors that reduce abrupt stalling. The inability to predict stall restricts the development of aggressive aerodynamic concepts.^[2]

Some blades (mostly on Enercon) have a winglet to increase performance and/or reduce noise.^{[18][19]}

A blade can have a lift-to-drag ratio of 120,^[20] compared to 70 for a sailplane and 15 for an airliner.^[21]

The hub

In simple designs, the blades are directly bolted to the hub and are unable to pitch, which leads to aerodynamic stall above certain windspeeds. In other more sophisticated designs, they are bolted to the pitch mechanism, which adjusts their angle of attack according to the wind speed to control their rotational speed. The pitch mechanism is itself bolted to the hub. The hub is fixed to the rotor shaft which drives the generator directly or through a gearbox.

Blade count

The number of blades is selected for aerodynamic efficiency, component costs, and system reliability. Noise emissions are affected by the location of the blades upwind or downwind of the tower and the speed of the rotor. Given that the noise emissions from the blades' trailing edges and tips vary by the 5th power of blade speed, a small increase in tip speed can make a large difference.

Wind turbines developed over the last 50 years have almost universally used either two or three blades. However, there are patents that present designs with additional blades, such as Chan Shin's Multi-unit rotor blade system integrated wind turbine.^[22] Aerodynamic efficiency increases with number of blades but with diminishing return. Increasing the number of blades from one to two yields a six percent increase in aerodynamic efficiency, whereas increasing the blade count from two to three yields only an additional three percent in efficiency.^[23] Further increasing the blade count yields minimal improvements in aerodynamic efficiency and sacrifices too much in blade stiffness as the blades become thinner.

Theoretically, an infinite number of blades of zero width is the most efficient, operating at a high value of the tip speed ratio. But other considerations lead to a compromise of only a few blades.^[24]



Unpainted tip of a blade



A Wind turbine hub being installed



The 98 meter diameter, two-bladed NASA/DOE Mod-5B wind turbine was the largest operating wind turbine in the world in the early 1990s

Component costs that are affected by blade count are primarily for materials and manufacturing of the turbine rotor and drive train. Generally, the lower the number of blades, the lower the material and manufacturing costs will be. In addition, the lower the number of blades, the higher the rotational speed can be. This is because blade stiffness requirements to avoid interference with the tower limit how thin the blades can be manufactured, but only for upwind machines; deflection of blades in a downwind machine results in increased tower clearance. Fewer blades with higher rotational speeds reduce peak torques in the drive train, resulting in lower gearbox and generator costs.



The NASA test of a one-bladed wind turbine rotor configuration at Plum Brook Station near Sandusky, Ohio

System reliability is affected by blade count primarily through the dynamic loading of the rotor into the drive train and tower systems. While aligning the wind turbine to changes in wind direction (yawing), each blade experiences a cyclic load at its root end depending on blade position. This is true of one, two, three blades or more. However, these cyclic loads when combined together at the drive train shaft are symmetrically balanced for three blades, yielding smoother operation during turbine yaw. Turbines with one or two blades can use a pivoting teetered hub to also nearly eliminate the cyclic loads into the drive shaft and system during yawing. A Chinese 3.6 MW two-blade is being tested in Denmark.^[25] Mingyang won a bid for 87 MW (29 * 3 MW) two-bladed offshore wind turbines near Zhuhai in 2013.^{[26][27][28]}

Finally, aesthetics can be considered a factor in that some people find that the three-bladed rotor is more pleasing to look at than a one- or two-bladed rotor.

Blade materials

In general, ideal materials should meet the following criteria:

- wide availability and easy processing to reduce cost and maintenance
- low weight or density to reduce gravitational forces
- high strength to withstand strong loading of wind and gravitational force of the blade itself
- high fatigue resistance to withstand cyclic loading
- high stiffness to ensure stability of the optimal shape and orientation of the blade and clearance with the tower
- high fracture toughness
- the ability to withstand environmental impacts such as lightning strikes, humidity, and temperature^[29]

This narrows down the list of acceptable materials. Metals would be undesirable because of their vulnerability to fatigue. Ceramics have low fracture toughness, which could result in early blade failure. Traditional polymers are not stiff enough to be useful, and wood has problems with repeatability, especially considering the length of the blade. That leaves fiber-reinforced composites, which have high strength and stiffness and low

density, as a very attractive class of materials for the design of wind turbines.^[30]

Wood and canvas sails were used on early windmills due to their low price, availability, and ease of manufacture. Smaller blades can be made from light metals such as aluminium. These materials, however, require frequent maintenance. Wood and canvas construction limits the airfoil shape to a flat plate, which has a relatively high ratio of drag to force captured (low aerodynamic efficiency) compared to solid airfoils. Construction of solid airfoil designs requires inflexible materials such as metals or composites. Some blades also have incorporated lightning conductors.

New wind turbine designs push power generation from the single megawatt range to upwards of 10 megawatts using larger and larger blades. A larger area effectively increases the tip-speed ratio of a turbine at a given wind speed, thus increasing its energy extraction.^[31] Computer-aided engineering software such as HyperSizer (originally developed for spacecraft design) can be used to improve blade design.^{[32][33]}

As of 2015 the rotor diameters of onshore wind turbine blades are as large as 130 meters,^[34] while the diameter of offshore turbines reach 170 meters.^[35] In 2001, an estimated 50 million kilograms of fibreglass laminate were used in wind turbine blades.^[36]

An important goal of larger blade systems is to control blade weight. Since blade mass scales as the cube of the turbine radius, loading due to gravity constrains systems with larger blades.^[37] Gravitational loads include axial and tensile/ compressive loads (top/bottom of rotation) as well as bending (lateral positions). The magnitude of these loads fluctuates cyclically and the edgewise moments (see below) are reversed every 180° of rotation. Typical rotor speeds and design life are ~10rpm and 20 years, respectively, with the number of lifetime revolutions on the order of 10^8 . Considering wind, it is expected that turbine blades go through ~ 10^9 loading cycles. Wind is another source of rotor blade loading. Lift causes bending in the flapwise direction (out of rotor plane) while air flow around the blade cause edgewise bending (in the rotor plane). Flapwise bending involves tension on the pressure (upwind) side and compression on the suction (downwind) side. Edgewise bending involves tension on the leading edge and compression on the trailing edge.

Wind loads are cyclical because of natural variability in wind speed and wind shear (higher speeds at top of rotation).

Failure in ultimate loading of wind-turbine rotor blades exposed to wind and gravity loading is a failure mode that needs to be considered when the rotor blades are designed. The wind speed that causes bending of the rotor blades exhibits a natural variability, and so does the stress response in the rotor blades. Also, the resistance of the rotor blades, in terms of their tensile strengths, exhibits a natural variability.^[38]

In light of these failure modes and increasingly larger blade systems, there has been continuous effort toward developing cost-effective materials with higher strength-to-mass ratios. In order to extend the current 20 year lifetime of blades and enable larger area blades to be cost-effective, the design and materials need to be optimized for stiffness, strength, and fatigue resistance.^[29]



Several modern wind turbines use rotor blades with carbon-fibre girders to reduce weight.

The majority of current commercialized wind turbine blades are made from fiber-reinforced polymers (FRP's), which are composites consisting of a polymer matrix and fibers. The long fibers provide longitudinal stiffness and strength, and the matrix provides fracture toughness, delamination strength, out-of-plane strength, and stiffness.^[29] Material indices based on maximizing power efficiency, and having high fracture toughness, fatigue resistance, and thermal stability, have been shown to be highest for glass and carbon fiber reinforced plastics (GFRP's and CFRPs).^[39]



Fiberglass-reinforced epoxy blades of Siemens SWT-2.3-101 wind turbines. The blade size of 49 meters^[40] is in comparison to a substation behind them at Wolfe Island Wind Farm.

Manufacturing blades in the 40 to 50 metre range involves proven fibreglass composite fabrication techniques. Manufacturers such as Nordex SE and GE Wind use an infusion process. Other manufacturers use variations on this technique, some including carbon and wood with fibreglass in an epoxy matrix. Other options include preimpregnated ("prepreg") fibreglass and vacuum-assisted resin transfer molding. Each of these options use a glass-fibre reinforced polymer composite constructed with differing complexity. Perhaps the largest issue with more simplistic, open-mould, wet systems are the emissions associated with the volatile organics released. Preimpregnated materials and resin infusion techniques avoid the release of volatiles by containing all VOC's. However, these contained processes have their own challenges, namely the production of thick laminates necessary for structural components becomes more difficult. As the preform resin permeability dictates the maximum laminate thickness, bleeding is required to eliminate voids and ensure proper resin distribution.^[36] One solution to resin distribution is a partially preimpregnated fibreglass. During evacuation, the dry fabric provides a path for airflow and, once heat and pressure are applied, resin may flow into the dry region resulting in a thoroughly impregnated laminate structure.^[36]

Epoxy-based composites have environmental, production, and cost advantages over other resin systems. Epoxies also allow shorter cure cycles, increased durability, and improved surface finish. Prepreg operations further reduce processing time over wet lay-up systems. As turbine blades pass 60 metres, infusion techniques become more prevalent; the traditional resin transfer moulding injection time is too long as compared to the resin set-up time, limiting laminate thickness. Injection forces resin through a thicker ply stack, thus depositing the resin where in the laminate structure before gelation occurs. Specialized epoxy resins have been developed to customize lifetimes and viscosity.^[41]

Carbon fibre-reinforced load-bearing spars can reduce weight and increase stiffness. Using carbon fibres in 60 metre turbine blades is estimated to reduce total blade mass by 38% and decrease cost by 14% compared to 100% fibreglass. Carbon fibres have the added benefit of reducing the thickness of fiberglass laminate sections, further addressing the problems associated with resin wetting of thick lay-up sections. Wind turbines may also benefit from the general trend of increasing use and decreasing cost of carbon fibre materials.^[36]

Although glass and carbon fibers have many optimal qualities for turbine blade performance, there are several downsides to these current fillers, including the fact that high filler fraction (10-70 wt%) causes increased

density as well as microscopic defects and voids that often lead to premature failure.^[29]

Recent developments include interest in using carbon nanotubes (CNT's) to reinforce polymer-based nanocomposites. CNT's can be grown or deposited on the fibers, or added into polymer resins as a matrix for FRP structures. Using nanoscale CNT's as filler instead of traditional microscale filler (such as glass or carbon fibers) results in CNT/polymer nanocomposites, for which the properties can be changed significantly at very low filler contents (typically < 5 wt%). They have very low density, and improve the elastic modulus, strength, and fracture toughness of the polymer matrix. The addition of CNT's to the matrix also reduces the propagation of interlaminar cracks which can be a problem in traditional FRP's.^[29]

Further improvement is possible through the use of carbon nanofibers (CNF's) in the blade coatings. A major problem in desert environments is erosion of the leading edges of blades by wind carrying sand, which increases roughness and decreases aerodynamic performance. The particle erosion resistance of fiber-reinforced polymers is poor when compared to metallic materials and elastomers, and needs to be improved. It has been shown that the replacement of glass fiber with CNF on the composite surface greatly improves erosion resistance. CNF's have also been shown to provide good electrical conductivity (important for lightning strikes), high damping ratio, and good impact-friction resistance. These properties make CNF-based nanopaper a prospective coating for wind turbine blades.^{[42][43]}

Blade recycling

The Global Wind Energy Council (GWEC) predicts that wind energy will supply 15.7% of the world's total energy needs by the year 2020, and 28.5% by the year 2030.^[44] This dramatic increase in global wind energy generation will require installation of a newer and larger fleet of more efficient wind turbines and the consequent decommissioning of aging ones. Based on a study carried out by the European Wind Energy Association, in the year 2010 alone, between 110 and 140 kilotons of composites were consumed by the wind turbine industry for manufacturing blades.^[45] The majority of the blade material will eventually end up as waste, and in order to accommodate this level of composite waste, the only option is recycling. Typically, glass-fibre-reinforced-polymers (GFRPs) compose of around 70% of the laminate material in the blade. GFRPs hinder incineration and are not combustible.^[46] Therefore, conventional recycling methods need to be modified. Currently, depending on whether individual fibres can be recovered, there exists a few general methods for recycling GFRPs in wind turbine blades:

- **Mechanical Recycling:** This method doesn't recover individual fibres. Initial processes involve shredding, crushing, and/or milling. The crushed pieces are then separated into fibre-rich and resin-rich fractions. These fractions are ultimately incorporated into new composites either as fillers or reinforcements.^[47]
- **Chemical Processing/Pyrolysis:** Thermal decomposition of the composites is used to recover the individual fibres. For pyrolysis, the material is heated up to 500 °C in an environment without oxygen, thus causing it to break down into lower weight organic substances and/or gaseous products. The glass fibres will generally lose 50% of their initial strength and can now be downcycled for fibre reinforcement applications in paints or concrete.^[48] Research has shown that this end of life option is able to recover up to approximately 19 MJ/kg.^[49] However, this method has a relatively high cost and requires similar mechanical pre-processing. In addition, it has not yet been modified to satisfy the future need of large scale wind turbine blade recycling.^[50]

Tower

Two main types of towers exist: floating towers and land-based towers, which are usually more common.

Tower height

Wind velocities increase at higher altitudes due to surface aerodynamic drag (by land or water surfaces) and the viscosity of the air. The variation in velocity with altitude, called wind shear, is most dramatic near the surface. Typically, the variation follows the wind profile power law, which predicts that wind speed rises proportionally to the seventh root of altitude. Doubling the altitude of a turbine, then, increases the expected wind speeds by 10% and the expected power by 34%. To avoid buckling, doubling the tower height generally requires doubling the diameter of the tower as well, increasing the amount of material by a factor of at least four.

At night time, or when the atmosphere becomes **stable**, wind speed close to the ground usually subsides whereas at turbine hub altitude it does not decrease that much or may even increase. As a result, the wind speed is higher and a turbine will produce more power than expected from the 1/7 power law: doubling the altitude may increase wind speed by 20% to 60%. A stable atmosphere is caused by radiative cooling of the surface and is common in a temperate climate: it usually occurs when there is a (partly) clear sky at night. When the (high altitude) wind is strong (a 10-meter wind speed higher than approximately 6 to 7 m/s) the stable atmosphere is disrupted because of friction turbulence and the atmosphere will turn **neutral**. A daytime atmosphere is either neutral (no net radiation; usually with strong winds and heavy clouding) or **unstable** (rising air because of ground heating—by the sun). Here again the 1/7 power law applies or is at least a good approximation of the wind profile. Indiana had been rated as having a wind capacity of 30,000 MW, but by raising the expected turbine height from 50 m to 70 m, the wind capacity estimate was raised to 40,000 MW, and could be double that at 100 m.^[51]

For HAWTs, tower heights approximately two to three times the blade length have been found to balance material costs of the tower against better utilisation of the more expensive active components.

Road size restrictions makes transportation of towers with a diameter of more than 4.3 m difficult. Swedish analyses show that it is important to have the bottom wing tip at least 30 m above the tree tops, but a taller tower requires a larger tower diameter.^[52] A 3 MW turbine may increase output from 5,000 MWh to 7,700 MWh per year by going from 80 to 125 meter tower height.^[53] A tower profile made of connected shells rather than cylinders can have a larger diameter and still be transportable. A 100 m prototype tower with TC bolted 18 mm 'plank' shells has been erected at the wind turbine test center Høvsøre in Denmark and certified by Det Norske Veritas, with a Siemens nacelle. Shell elements can be shipped in standard 12 m shipping containers,^{[52][54]} and 2½ towers per week are produced this way.^[55]

As of 2003, typical modern wind turbine installations use towers about 210 ft (65 m) high. Height is typically limited by the availability of cranes. This has led to a variety of proposals for "partially self-erecting wind turbines" that, for a given available crane, allow taller towers that put a turbine in stronger and steadier winds, and "self-erecting wind turbines" that can be installed without cranes.^{[56][57][58][59]}

Tower materials

Currently, the majority of wind turbines are supported by conical tubular steel towers. These towers represent



Sections of a wind turbine tower, transported in a bulk carrier ship

30% – 65% of the turbine weight and therefore account for a large percentage of the turbine transportation costs. The use of lighter materials in the tower could greatly reduce the overall transport and construction cost of wind turbines, however the stability must be maintained.^[60] Higher grade S500 steel costs 20%-25% more than S335 steel (standard structural steel), but it requires 30% less material because of its improved strength. Therefore, replacing wind turbine towers with S500 steel would result in a net savings in both weight and cost.^[61]

Another disadvantage of conical steel towers is that constructing towers that meet the requirements of wind turbines taller than 90 meters proves challenging. High performance concrete shows potential to increase tower height and increase the lifetime of the towers. A hybrid of prestressed concrete and steel has shown improved performance over standard tubular steel at tower heights of 120 meters.^[62] Concrete also gives the benefit of allowing for small precast sections to be assembled on site, avoiding the challenges steel faces during transportation.^[63] One downside of concrete towers is the higher CO2 emissions during concrete production as compared to steel. However, the overall environmental benefit should be higher if concrete towers can double the wind turbine lifetime.^[64]

Wood is being investigated as a material for wind turbine towers, and a 100 metre tall tower supporting a 1.5 MW turbine has been erected in Germany. The wood tower shares the same transportation benefits of the segmented steel shell tower, but without the steel resource consumption.^{[65][66]}

Connection to the electric grid

All grid-connected wind turbines, from the first one in 1939 until the development of variable-speed grid-connected wind turbines in the 1970s, were fixed-speed wind turbines. As recently as 2003, nearly all grid-connected wind turbines operated at exactly constant speed (synchronous generators) or within a few percent of constant speed (induction generators).^{[67][68]} As of 2011, many operational wind turbines used fixed speed induction generators (FSIG).^[69] As of 2011, most new grid-connected wind turbines are variable speed wind turbines—they are in some variable speed configuration.^[69]

Early wind turbine control systems were designed for peak power extraction, also called maximum power point tracking—they attempt to pull the maximum possible electrical power from a given wind turbine under the current wind conditions.^[70] More recent wind turbine control systems deliberately pull less electrical power than they possibly could in most circumstances, in order to provide other benefits, which include:

- spinning reserves to quickly produce more power when needed—such as when some other generator suddenly drops from the grid—up to the max power supported by the current wind conditions.^[71]
- Variable-speed wind turbines can (very briefly) produce more power than the current wind conditions can support, by storing some wind energy as kinetic energy (accelerating during brief gusts of faster wind) and later converting that kinetic energy to electric energy (decelerating, either when more power is needed elsewhere, or during short lulls in the wind, or both).^{[72][73]}
- damping (electrical) subsynchronous resonances in the grid^[74]
- damping (mechanical) resonances in the tower^{[75][76]}

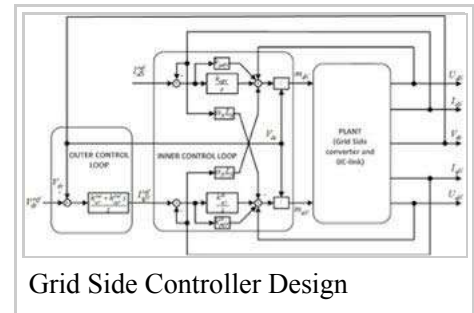
The generator in a wind turbine produces alternating current (AC) electricity. Some turbines drive an AC/AC converter—which converts the AC to direct current (DC) with a rectifier and then back to AC with an inverter—in order to match the frequency and phase of the grid. However, the most common method in large modern turbines is to instead use a doubly fed induction generator directly connected to the electricity grid.

A useful technique to connect a permanent magnet synchronous generator to the grid is by using a back-to-back converter. Also, we can have control schemes so as to achieve unity power factor in the connection to the grid. In that way the wind turbine will not consume reactive power, which is the most common problem with wind turbines that use induction machines. This leads to a more stable power system. Moreover, with different control schemes a wind turbine with a permanent magnet synchronous generator can provide or consume reactive power. So, it can work as a dynamic capacitor/inductor bank so as to help with the power systems' stability.

Below we show the control scheme so as to achieve unity power factor :

Reactive power regulation consists of one PI controller in order to achieve operation with unity power factor (i.e. $Q_{\text{grid}} = 0$). It is obvious that I_{dN} has to be regulated to reach zero at steady-state ($I_{dN\text{ref}} = 0$).

We can see the complete system of the grid side converter and the cascaded PI controller loops in the figure in the right.

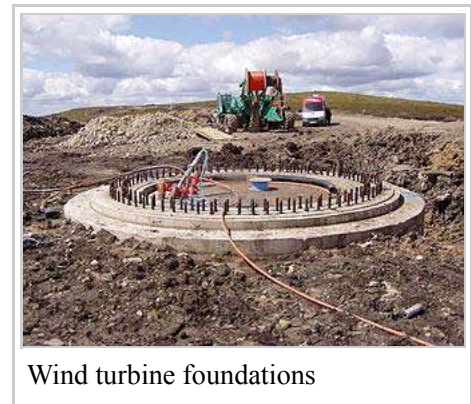


Grid Side Controller Design

Foundations

Wind turbines, by their nature, are very tall slender structures,^[77] this can cause a number of issues when the structural design of the foundations are considered.

The foundations for a conventional engineering structure are designed mainly to transfer the vertical load (dead weight) to the ground, this generally allows for a comparatively unsophisticated arrangement to be used. However, in the case of wind turbines, due to the high wind and environmental loads experienced there is a significant horizontal dynamic load that needs to be appropriately restrained.



Wind turbine foundations

This loading regime causes large moment loads to be applied to the foundations of a wind turbine. As a result, considerable attention needs to be given when designing the footings to ensure that the turbines are sufficiently restrained to operate efficiently.^[78] In the current Det Norske Veritas (DNV) guidelines for the design of wind turbines the angular deflection of the foundations are limited to 0.5° .^[79] DNV guidelines regarding earthquakes suggest that horizontal loads are larger than vertical loads for offshore wind turbines, while guidelines for tsunamis only suggest designing for maximum sea waves.^[80] In contrast, IEC suggests considering tsunami loads.^[81]

Scale model tests using a 50-g centrifuge are being performed at the Technical University of Denmark to test monopile foundations for offshore wind turbines at 30 to 50-m water depth.^[82]

Costs

The modern wind turbine is a complex and integrated system. Structural elements comprise the majority of the weight and cost. All parts of the structure must be inexpensive, lightweight, durable, and manufacturable, under variable loading and environmental conditions. Turbine systems that have fewer failures,^[85] require less maintenance, are lighter and last longer will lead to reducing the cost of wind energy.

One way to achieve this is to implement well-documented, validated analysis codes, according to a 2011 report from a coalition of researchers from universities, industry, and government, supported by the Atkinson Center for a Sustainable Future.^[2]

The major parts of a modern turbine may cost (percentage of total): tower 22%, blades 18%, gearbox 14%, generator 8%.^{[86][87]}

Efficiency and wind speed

The efficiency of a wind turbine is maximum at its design wind velocity, and efficiency decreases with the fluctuations in wind. The lowest velocity at which the turbine develops its full power is known as rated wind velocity. Below some minimum wind velocity, no useful power output can be produced from wind turbine. There are limits on both the minimum (2–5 m/s) and maximum (25–30 m/s) wind velocity for the efficient operation of wind turbines.^{[88][89]}

Conservation of mass requires that the amount of air entering and exiting a turbine must be equal. Accordingly, Betz's law gives the maximal achievable extraction of wind power by a wind turbine as 16/27 (59.3%) of the total kinetic energy of the air flowing through the turbine.^[90]

The maximum theoretical power output of a wind machine is thus 0.59 times the kinetic energy of the air passing through the effective disk area of the machine. If the effective area of the disk is *A*, and the wind velocity *v*, the maximum theoretical power output *P* is:

$$P = 0.59 \frac{1}{2} \rho v^3 A$$

where *ρ* is air density

As wind is free (no fuel cost), wind-to-rotor efficiency (including rotor blade friction and drag) is one of many aspects impacting the final price of wind power.^[91] Further inefficiencies, such as gearbox losses, generator and converter losses, reduce the power delivered by a wind turbine. To protect components from undue wear, extracted power is held constant above the rated operating speed as theoretical power increases at the cube of wind speed, further reducing theoretical efficiency. In 2001, commercial utility-connected turbines deliver 75% to 80% of the Betz limit of power extractable from the wind, at rated operating speed.^{[89][92]}

All power plants have some consumption when they produce power, and some standby consumption when they are turned on without producing power. For a modern 3 MW wind turbine, the consumption may be 6-58 kW depending on circumstances.^[93]

Design specification

The design specification for a wind-turbine will contain a power curve and guaranteed availability. With the data from the wind resource assessment it is possible to calculate commercial viability.^[1] The typical operating temperature range is −20 to 40 °C (−4 to 104 °F). In areas with extreme climate (like Inner Mongolia or Rajasthan) specific cold and hot weather versions are required.



Liftra *Blade Dragon* installing a single blade on wind turbine hub.^{[83][84]}

Wind turbines can be designed and validated according to IEC 61400 standards.^[81]

Low temperature

Utility-scale wind turbine generators have minimum temperature operating limits which apply in areas that experience temperatures below -20 °C . Wind turbines must be protected from ice accumulation. It can make anemometer readings inaccurate and which, in certain turbine control designs, can cause high structure loads and damage. Some turbine manufacturers offer low-temperature packages at a few percent extra cost, which include internal heaters, different lubricants, and different alloys for structural elements. If the low-temperature interval is combined with a low-wind condition, the wind turbine will require an external supply of power, equivalent to a few percent of its rated power, for internal heating. For example, the St. Leon, Manitoba project has a total rating of 99 MW and is estimated to need up to 3 MW (around 3% of capacity) of station service power a few days a year for temperatures down to -30 °C . This factor affects the economics of wind turbine operation in cold climates.

See also

- Brushless wound-rotor doubly fed electric machine
- Floating wind turbine
- Vertical-axis wind turbine
- Wind-turbine aerodynamics

References

1. "Efficiency and performance" (PDF). UK Department for Business, Enterprise & Regulatory Reform. Retrieved 2007-12-29.
2. Alan T. Zehnder & Zellman Warhaft (27 July 2011). "University Collaboration on Wind Energy" (PDF). Cornell University Atkinson Center for a Sustainable Future. Retrieved 22 August 2011.
3. Johnson, Scott J.; van Dam, C.P.; Berg, Dale E. (2008). "Active Load Control Techniques for Wind Turbines" (PDF). Sandia National Laboratory. Retrieved 13 September 2009.
4. "What factors affect the output of wind turbines?". *Alternative-energy-news.info*. 2009-07-24. Retrieved 2013-11-06.
5. Sagrillo, Mick (2010). "SMALL TURBINE COLUMN" (PDF). *Windletter*. **29** (1). Retrieved 19 December 2011.
6. "Vestas world's largest wind turbines". *Renewableenergyfocus.com*. 2010-10-24. Retrieved 2013-11-06.
7. "How It Works: Gearless wind Turbine". *Popsci.com*. 2010-03-26. Retrieved 2013-11-06.
8. "The global wind energy market gears up for growth (<http://www.power-technology.com/features/feature-global-wind-energy-market-gears-growth/>)" *Power Technology / GlobalData*, 18 September 2013 . Accessed: 16 October 2013.
9. "Could Magnetic Gears Make Wind Turbines Say Goodbye to Mechanical Gearboxes?". *machinedesign.com*.
10. Navid Goudarzi (June 2013). "A Review on the Development of the Wind Turbine Generators across the World". *International Journal of Dynamics and Control*. Springer. **1** (2): 192–202. doi:10.1007/s40435-013-0016-y.
11. Text und Photos: ENERCON Germany www.enercon.de. "Anatomy of an Enercon direct drive wind turbine". *Wwindea.org*. Retrieved 2013-11-06.
12. Fairly, Peter. Wind Turbines Shed Their Gears (<http://www.technologyreview.com/energy/25188/>) *Technology Review*, 27 April 2010. Retrieved: 22 September 2010.
13. Wittrup, Sanne. First Siemens gearless (<http://ing.dk/artikel/110879-gearloese-moeller-fra-siemens-bliver-solgt-for-foerste-gang>) *Ing.dk*, 11 August 2010. Retrieved: 15 September 2010.
14. Wittrup, Sanne. 6MW Siemens gearless (<http://ing.dk/artikel/111960-siemens-udvikler-6-mw-gearloes-moelle>) *Ing.dk*, 15 September 2010. Retrieved: 15 September 2010.

15. reliawind.eu (<http://www.reliawind.eu>)
16. Wittrup, Sanne. PMs cause production problems (<http://ing.dk/artikel/123609-permanente-magneter-volder-vestas-problemer-i-produktionen>) English translation (http://translate.google.dk/translate?sl=da&tl=en&js=n&prev=_t&hl=da&ie=UTF-8&layout=2&eotf=1&u=http%3A%2F%2Fing.dk%2Fartikel%2F123609-permanente-magneter-volder-vestas-problemer-i-produktionen) *Ing.dk*, 1 November 2011. Accessed: 1 November 2011.
17. Chu, Steven. Critical Materials Strategy (http://energy.gov/sites/prod/files/DOE_CMS_2011.pdf) *United States Department of Energy*, December 2011. Accessed: 23 December 2011.
18. Hau, Erich. "Wind Turbines: Fundamentals, Technologies, Application, Economics" p142. Springer Science & Business Media, 26. feb. 2013. ISBN 3642271510
19. <http://www.windpowermonthly.com/article/1133706/enercons-direct-drive-evolution>
20. Jamieson, Peter. Innovation in Wind Turbine Design (<https://books.google.dk/books?id=HyUIpGPO-k0C&printsec=frontcover&hl=da>) sec11-1, *John Wiley & Sons*, 5 July 2011. Accessed: 26 February 2012. ISBN 1-119-97545-X
21. Kroo, Ilan. NASA Green Aviation Summit (http://www.aeronautics.nasa.gov/pdf/23_kroo_green_aviation_summit.pdf) p9, *NASA*, September 2010. Accessed: 26 February 2012.
22. "Patent US5876181 - Multi-unit rotor blade system integrated wind turbine - Google Patents". Google.com. Retrieved 2013-11-06.
23. Eric Hau (ed), *Wind Turbines Fundamentals, Technologies, Applications, Economics 2nd Edition*, Springer 2006, ISBN 3-540-24240-6 page 121
24. Hugh Piggott (1998). "CAT windpower course Blade design notes" (PDF).. Course notes from Scoraig Wind Electric, used in courses at the Centre for Alternative Technology.
25. Boel, Thomas (22 November 2012). "Two wings work". *Ingeniøren*. Retrieved 22 November 2012. Design (<http://ing.dk/artikel/134390-se-detaljerne-paa-kinesisk-moelle-med-kun-to-vinger#0>)
26. "MY Secures Off-Shore Tender in Zhuhai, Guangdong Province, China with 3MW SCD Wind Turbine Generators, Construction to Begin in October 2013 (<http://www.wspa.com/story/23564370/my-secures-off-shore-tender-in-zhuhai-guangdong-province-china-with-3mw-scd-wind-turbine-generators-construction-to-begin-in-october-2013>)" *WSPA*, 30 September 2013. Accessed: 22 November 2013.
27. "2.5/2.75/3.0MW Series Wind Turbine Generator (<http://www.mywind.com.cn/English/program/products.aspx?MenuID=05030301&ID=30>)" *Ming Yang*. Accessed: 22 November 2013.
28. "4c Zhuhai (<http://www.4coffshore.com/windfarms/zhuhai-guishan-offshore-wind-farm-demonstration-project-china-cn86.html>)"
29. Ma, P., & Zhang, Y. *Perspectives of carbon nanotubes/polymer nanocomposites for wind blade materials*. In: *Renewable and Sustainable Energy Reviews*, 30, (2014), 651-660, doi:10.1016/j.rser.2013.11.008 (<https://dx.doi.org/10.1016%2Fj.rser.2013.11.008>).
30. <http://www.uotechnology.edu.iq/dep-laserandoptoelec-eng/branch/lectures/solid%20state/chapter%201%20classification%20of%20materail.pdf>
31. Zbigniew Lubosny (2003). *Wind Turbine Operation in Electric Power Systems: Advanced Modeling (Power Systems)*. Berlin: Springer. ISBN 3-540-40340-X.
32. "Materials and design methods look for the 100-m blade". *Windpower Engineering*. 10 May 2011. Retrieved 22 August 2011.
33. Craig S. Collier (1 October 2010). "From Aircraft Wings to Wind Turbine Blades: NASA Software Comes Back to Earth with Green Energy Applications". *NASA Tech Briefs*. Retrieved 22 August 2011.
34. Nordex secures first N131/3000 in Finland (<http://www.windpowermonthly.com/article/1333448/nordex-secures-first-n131-3000-finland>) In: *Windpower Monthly*, Retrieved 22. February 2015.
35. *Weltgrößte Offshore-Turbine errichtet* (<http://www.erneuerbareenergien.de/weltgroesste-offshore-turbine-errichtet/150/469/74200/>). In: *Erneuerbare Energien. Das Magazin* Retrieved 22. February 2015.
36. Griffin, Dayton A.; Ashwill, Thomas D. (2003). "Alternative Composite Materials for Megawatt-Scale Wind Turbine Blades: Design Considerations and Recommended Testing". *Journal of Solar Energy Engineering*. **125** (4): 515. doi:10.1115/1.1629750.
37. Ashwill, T; Laird D (January 2007). *Concepts to Facilitate Very Large Blades* (PDF). 45th AIAA Aerospace Sciences Meeting and Exhibit. AIAA-2007-0817.
38. Ronold, K. O., & Larsen, G. C. (2000). Reliability-based design of wind-turbine rotor blades against failure in ultimate loading. *Engineering Structures*, 22(6), 565-574.
39. Bassyouni, M., & Gutub, S. A. (2013). Materials selection strategy and surface treatment of polymer composites for wind turbine blades fabrication. *Polymers & Polymer Composites*, 21, 463-471.

40. "Aerodynamic and Performance Measurements on a SWT-2.3- 101 Wind Turbine" (PDF). *WINDPOWER 2011*. National Renewable Energy Laboratory. 22–25 May 2011. p. 1. Retrieved 14 October 2013.
41. Christou, P (2007). "Advanced materials for turbine blade manufacture". *Reinforced Plastics*. **51** (4): 22. doi:10.1016/S0034-3617(07)70148-0.
42. Zhang, N., Yang, F., Guerra, D., Shen, C., Castro, J., & Lee, J. L. (2013). Enhancing particle erosion resistance of glass-reinforced polymeric composites using carbon nanofiber-based nanopaper coatings. *Journal of Applied Polymer Science*, 129(4), 1875-1881.
43. Liang, F., Tang, Y., Gou, J., & Kapat, J. (2011). Development of multifunctional nanocomposite coatings for wind turbine blades. *Ceramic Transactions*, 224, 325-336.
44. "GLOBAL WIND ENERGY OUTLOOK 2008 | GWEC". *www.gwec.net*. Retrieved 2016-11-07.
45. The European Wind Energy Association. "Research note outline on recycling wind turbines blades" (PDF).
46. Duflou, Joost R.; Deng, Yelin; Acker, Karel Van; Dewulf, Wim (2012-04-01). "Do fiber-reinforced polymer composites provide environmentally benign alternatives? A life-cycle-assessment-based study". *MRS Bulletin*. **37** (4): 374–382. doi:10.1557/mrs.2012.33. ISSN 1938-1425.
47. Pickering, S. J. (2006-08-01). "Recycling technologies for thermoset composite materials—current status". *Composites Part A: Applied Science and Manufacturing*. The 2nd International Conference: Advanced Polymer Composites for Structural Applications in Construction. **37** (8): 1206–1215. doi:10.1016/j.compositesa.2005.05.030.
48. "Recycling of wind turbine blades - Appropedia: The sustainability wiki". *www.appropedia.org*. Retrieved 2016-11-08.
49. Duflou, Joost R.; Deng, Yelin; Acker, Karel Van; Dewulf, Wim (2012-04-01). "Do fiber-reinforced polymer composites provide environmentally benign alternatives? A life-cycle-assessment-based study". *MRS Bulletin*. **37** (4): 374–382. doi:10.1557/mrs.2012.33. ISSN 1938-1425.
50. "ReFiber ApS Wind Turbine Blade Recycling Technology".
51. "Indiana's Renewable Energy Resources". *Indianacleanpower.org*. 2013-08-07. Retrieved 2013-11-06.
52. Emme, Svend. New type of wind turbine tower (<http://www.jernindustri.dk/artikel/VisArtikel.aspx?SiteID=JM&Lopenr=108300013&newsletterRefID=6173>) *Metal Industry*, 8 August 2011. Accessed: 10 December 2011.
53. Wittrup, Sanne. Ny type vindmølleårn samles af lameller (<http://ing.dk/artikel/ny-type-vindmolletårn-samles-af-lameller-123516>), *Ingeniøren*, 29. October 2011. Accessed: 12 May 2013.
54. "The shell tower in brief (<http://andresen-towers.com/concept>)". *Andresen Towers*. Retrieved: 13 November 2012.
55. Lund, Morten. Robotter bag dansk succes med vindmølleårne (<http://ing.dk/artikel/robotter-bag-dansk-succes-med-vindmoelletaarne-158563>), *Ingeniøren*, 12 May 2013. Accessed: 12 May 2013.
56. "WindPACT Turbine Design: Scaling Studies Technical Area 3 -- Self-Erecting Tower and Nacelle Feasibility" (<http://www.nrel.gov/docs/fy01osti/29493.pdf>). 2001.
57. R. D. Fredrickson. "A self-erecting method for wind turbines." (<https://www.xcelenergy.com/staticfiles/xcel/Corporate/Renewable%20Energy%20Grants/BlattnerSelfErectingWindTurbine2005Report.pdf>). 2003.
58. Nic Sharpley. "What's holding up tower technology?" (<http://www.windpowerengineering.com/featured/business-news-projects/whats-holding-up-tower-technology/>). 2013.
59. "Self-Erecting Wind Turbine Designed for Remote Sites" (<http://www.renewableenergyworld.com/articles/2002/01/self-erecting-wind-turbine-designed-for-remote-sites-5785.html>). 2002.
60. Ancona, Dan, and Jim McVeigh. (2011): Wind Turbine - Materials and Manufacturing Fact Sheet. Princeton Energy Resources International, LLC, 19 Aug. 2001. Web. 21 Oct. 2015. <http://www.perihq.com/documents/WindTurbine-MaterialsandManufacturing_FactSheet.pdf>.
61. ""Steel Solutions in the Green Economy." (2015): Wind Turbines. World Steel Association, 2012. Web. 21 Oct. 2015. <<https://www.worldsteel.org/dms/internetDocumentList/bookshop/worldsteel-wind-turbines-web/document/Steel%20solutions%20in%20the%20green%20economy:%20Wind%20turbines.pdf>>.
62. Quilligan, Aidan, A. O'Connor, and V. Pakrashi. "Fragility analysis of steel and concrete wind turbine towers." *Engineering Structures* 36 (2012): 270-282.
63. http://www.ecocem.ie/downloads/Concrete_Windmills.pdf
64. Levitan, Dave. "Too Tall for Steel: Engineers Look to Concrete to Take Wind Turbine Design to New Heights." *IEEE Spectrum*, 16 May 2013. Web. 21 Oct. 2015. <<http://spectrum.ieee.org/energywise/green-tech/wind/too-tall-for-steel-engineers-look-to-concrete-to-take-wind-turbine-design-to-new-heights>>.
65. McGar, Justin. "Wind Power Revolution: The World's First Timber Turbine" (<http://designbuildsource.com.au/wind-power-revolution-worlds-timber-turbine/>) *Design Build Source*, 13 November 2012. Retrieved: 13 November 2012.
66. RICHARDSON, JAKE. "99% Natural Timber Tower for Wind Turbines" (<http://cleantechnica.com/2012/10/18/99-natural-timber-tower-provides-wind-power/>) *Clean Technica*, 18 October 2012. Retrieved: 13 November 2012.

67. P. W. Carlin, A. S. Laxson, and E. B. Muljadi. "The History and State of the Art of Variable-Speed wind Turbine Technology" (http://geosci.uchicago.edu/~moyer/GEOS24705/Readings/Carlin_VariableSpeed.pdf). 2003. p. 130-131.
68. Murthy, S.S.; Singh, B.; Goel, P.K.; Tiwari, S.K. "A Comparative Study of Fixed Speed and Variable Speed Wind Energy Conversion Systems Feeding the Grid" (http://ieeexplore.ieee.org/xpl/login.jsp?tp=&arnumber=4487785&url=http%3A%2F%2Fieeexplore.ieee.org%2Fxppls%2Fabs_all.jsp%3Farnumber%3D4487785). 2007. doi: 10.1109/PEDS.2007.4487785
69. Nolan D. Caliao. "Dynamic modelling and control of fully rated converter wind turbines" (<http://www.sciencedirect.com/science/article/pii/S0960148111000048>). "Renewable Energy" 2011. doi: 10.1016/j.renene.2010.12.025
70. Ali M. Eltamaly, A. I. Alolah, and Hassan M. Farh. "Maximum Power Extraction from Utility-Interfaced Wind Turbines" (<http://www.intechopen.com/books/new-developments-in-renewable-energy/maximum-power-extraction-from-utility-interfaced-wind-turbines>). 2013. DOI: 10.5772/54675
71. E. Muljadi, M. Singh, and V. Gevorgian. "Fixed-Speed and Variable-Slip Wind Turbines Providing Spinning Reserves to the Grid" (<http://www.nrel.gov/docs/fy13osti/56817.pdf>). In "New Developments in Renewable Energy" (<http://www.intechopen.com/books/new-developments-in-renewable-energy>). 2013.
72. E. Muljadi and C.P. Butterfield. "Pitch-Controlled Variable-Speed Wind Turbine Generation" (<http://www.nrel.gov/docs/fy00osti/27143.pdf>). 1999.
73. E. Muljadi, K. Pierce, and P. Migliore. "A Conservative Control Strategy for Variable-Speed Stall-Regulated Wind Turbines" (<https://calpoly-wind-turbine.googlecode.com/hg/Research/A%20Conservative%20Control%20Strategy%20for%20Var%20Speed%20Stall%20Reg%20WT.pdf>). 2000.
74. Ewais, A.M.; Liang, J.; Ekanayake, J.B.; Jenkins, N. "Influence of Fully Rated Converter-based wind turbines on SSR" (http://ieeexplore.ieee.org/xpl/login.jsp?tp=&arnumber=6303160&url=http%3A%2F%2Fieeexplore.ieee.org%2Fxppls%2Fabs_all.jsp%3Farnumber%3D6303160). 2012. doi: 10.1109/ISGT-Asia.2012.6303160
75. Mate Jelavić, Nedjeljko Perić, Ivan Petrović. "Damping of Wind Turbine Tower Oscillations through Rotor Speed Control" (<http://act.rasip.fer.hr/materijali/11/EVER07-paper-34.pdf>). 2007.
76. A. Rodríguez T., C. E. Carcangiu, I. Pineda, T. Fischer, B. Kuhnle, M. Scheu, M. Martin. "Wind Turbine Structural Damping Control for Tower Load Reduction" (http://link.springer.com/chapter/10.1007/978-1-4419-9316-8_12). 2011. doi: 10.1007/978-1-4419-9316-8_12
77. Lombardi, D. (2010). Long Term Performance of Mono-pile Supported Offshore Wind Turbines. Bristol: University of Bristol.
78. Cox, J. A., & Jones, C. (2010). Long-Term Performance of Suction Caisson Supported Offshore Wind Turbines. Bristol: University of Bristol.
79. Det Norske Veritas (2001). *Guidelines for Design of Wind Turbines*. Copenhagen: Det Norske Veritas.
80. DNV-OS-J101 Design of Offshore Wind Turbine Structures (http://exchange.dnv.com:6389/dynaweb/offshore/os-j101/@Generic__BookTextView/11341;hf=0;cs=default;ts=default) *Det Norske Veritas*. Accessed: 12 March 2011.
81. International Standard IEC 61400-1, Third Edition (http://webstore.iec.ch/preview/info_iec61400-1%7Bed3.0%7Den.pdf) *International Electrotechnical Commission*, August 2005. Accessed: 12 March 2011.
82. Rasmussen, Daniel. Wind turbine foundations at 50g (<http://ing.dk/artikel/113038-centrifuge-paa-dtu-tester-moellefundamenter-ved-50-g>) (in Danish) *Ing.dk*, 26 October 2010. 6minute Video (<http://ing.dk/artikel/113041-se-dtus-centrifuge-skabe-50-g>) Retrieved: 25 November 2010.
83. "Blade Dragon". State of Green. Retrieved 13 December 2012.
84. R. Simonsen, Torben. "Liftra indstiller Blade Dragon". Retrieved 13 December 2012.
85. Budny, Rob. Bearing Failures Cause Serious Problems for Wind Turbines, but There Are Solutions (<http://machinedesign.com/mechanical-drives/bearing-failures-cause-serious-problems-wind-turbines-there-are-solutions>) | Machine Design Magazine, 26 June 2014.
86. Jamieson, Peter. Innovation in Wind Turbine Design (<https://books.google.dk/books?id=qCAwt6Tgga4C&printsec=frontcover&hl=da>) p155, *John Wiley & Sons*, 7 July 2011. Accessed: 26 February 2012. ISBN 0-470-69981-7
87. Jamieson, Peter. Innovation in Wind Turbine Design (<https://books.google.dk/books?id=rf9C33rGR1wC&printsec=frontcover&hl=da>) sec9-1, *John Wiley & Sons*, 7 July 2011. Accessed: 26 February 2012. ISBN 1-119-97612-X

88. Hau, E.--(Erich), Snel, Herman (2000). *Large wind turbines*. Wiley, Chichester, New York. ISBN 0471494569.
89. "Enercon E-family, 330 Kw to 7.5 Mw, Wind Turbine Specification" (http://www.enercon.de/p/downloads/EN_Productoverview_0710.pdf) Archived (https://web.archive.org/web/20110516022444/http://www.enercon.de/p/downloads/EN_Productoverview_0710.pdf) May 16, 2011, at the Wayback Machine.
90. "The Physics of Wind Turbines Kira Grogg Carleton College, 2005, p.8" (PDF). Retrieved 2013-11-06.
91. "Wind Energy Basics". Bureau of Land Management. Retrieved 23 April 2016.
92. Tony Burton et al., (ed), *Wind Energy Handbook*, John Wiley and Sons 2001 ISBN 0471489972 page 65
93. Her får vindmøllene penger for å skru seg av (<http://www.tu.no/artikler/her-far-vindmollene-penger-for-a-skru-seg-av/358610>) *Teknisk Ukeblad*, September 2016.

Further reading

- Robert Gasch, Jochen Twele (ed.), *Wind power plants. Fundamentals, design, construction and operation*, Springer 2012 ISBN 978-3-642-22937-4.
- Paul Gipe, ed. (2004). *Wind Power: Renewable Energy for Home, Farm, and Business* (second ed.). Chelsea Green Publishing Company. ISBN 978-1-931498-14-2.
- Erich Hau, *Wind turbines: fundamentals, technologies, application, economics* Springer, 2013 ISBN 978-3-642-27150-2 (preview on Google Books)
- Siegfried Heier, *Grid integration of wind energy conversion systems* Wiley 2006, ISBN 978-0-470-86899-7.
- Peter Jamieson, *Innovation in Wind Turbine Design*. Wiley & Sons 2011, ISBN 978-0-470-69981-2
- David Spera (ed.) *Wind Turbine Technology: Fundamental Concepts in Wind Turbine Engineering*, Second Edition (2009), ASME Press, ISBN 9780791802601
- Alois Schaffarczyk (ed.), *Understanding wind power technology*, Wiley & Sons 2014, ISBN 978-1-118-64751-6.
- Wei Tong, ed. (2010). *Wind Power Generation and Wind Turbine Design*. WIT Press. ISBN 978-1-84564-205-1.
- Hermann-Josef Wagner, Jyotirmay Mathur, *Introduction to wind energy systems. Basics, technology and operation*. Springer 2013, ISBN 978-3-642-32975-3.

External links

- Offshore Wind Turbines - Installation and Operation of Turbines (<http://www.brighthub.com/environment/renewable-energy/articles/63997.aspx>)
- Department of Energy- Energy Efficiency and Renewable Energy (<http://www.eere.energy.gov/>)
- RenewableUK - Wind Energy Reference and FAQs (<http://www.bwea.com/ref/faq.html#efficient/>)
- How is Wind turbine made (<http://www.madehow.com/Volume-1/Wind-Turbine.html>)



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